## Traffic Impact Study for Stony Oaks Apartments



Prepared for the City of Santa Rosa

Submitted by
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## Executive Summary

The proposed Stony Oaks project consists of a 142-unit affordable apartments complex to be located on a currently vacant site at 2542 Old Stony Point Road in the City of Santa Rosa. The project would take access from a driveway on Old Stony Point Road as well as a driveway on Hearn Avenue. The project would be expected to generate 772 trips per day, including 51 trips during the weekday a.m. peak hour and 62 trips during the weekday p.m. peak hour.

Analysis indicates that four of the five study intersections operate acceptably per the applicable City standards under Existing and Baseline Conditions and would continue to do so with the addition of project traffic. The intersection at Hearn Avenue/Burbank Avenue would operate acceptably overall under Existing and Existing plus Project conditions, though would encounter LOS E or F operation on the stop-controlled southbound leg; the peak hour signal warrant would remain unmet. Under Baseline and Baseline plus Project conditions, delays at the intersection would increase, and the peak hour signal warrant would be met both without and with the proposed project. The proposed project would be expected to increase overall delays at the intersection by 1.7 to 2.2 seconds under Baseline conditions, which falls below the City's significance criteria of five seconds. The City of Santa Rosa plans to signalize the intersection as detailed in the 2016 Roseland Area/Sebastopol Road Specific Plan. Installation of a signal would be expected improve LOS to acceptable levels under both near-term and long-range conditions. As indicated by the City, the project should contribute its proportionate share of $\$ 29,760$ toward signalization of the intersection.

The project site is in an area of Santa Rosa that has a baseline residential VMT per capita that is more than 15 percent below the Countywide average, falling below the City's significance thresholds contained in the Vehicle Miles Traveled (VMT) Guidelines Final Draft. As a 100 percent affordable residential development, the project also qualifies for VMT screening criteria established by the City of Santa Rosa. Given these conditions, the project may be presumed to have a less than significant VMT impact.

Existing pedestrian and bicycle facilities in the project vicinity, including sidewalks and Class II bike lanes on Hearn Avenue and Stony Point Road, will adequately serve these modes upon completion of the sidewalk frontage improvements to be installed as part of the project. Santa Rosa CityBus transit routes also operate within a walkable distance of the project site and would be accessible via the sidewalk system. Project residents would be able to walk to surrounding areas and transit stops via the project's connection to Old Stony Point Road and existing sidewalk facilities including those on the south side of Hearn Avenue. Additional pedestrian connectivity options would exist in the future once continuous sidewalks are constructed on adjacent properties along the north side of Hearn Avenue.

Sight lines are currently adequate at the project driveways to accommodate all turns into and out of the site. To maintain existing sight lines, it is recommended that any new signage and taller landscaping to be installed along the project frontage be placed outside of the vision triangle of a driver waiting on each driveway. The site would provide effective access and circulation for emergency response vehicles.

The project would qualify for State density bonus provisions that require a minimum of 185 parking spaces, which equals the proposed supply. The project would provide both long-term and short-term bicycle parking in excess of that required by the City's zoning code.

## Introduction

This report presents an analysis of the potential traffic impacts that would be associated with development of the proposed Stony Oaks Apartments project to be located at 2542 Old Stony Point Road in the City of Santa Rosa. The traffic study was completed in accordance with the criteria established by the City of Santa Rosa, reflects a scope of work and study area reviewed and approved by City staff, and is consistent with standard traffic engineering techniques.

## Prelude

The purpose of a traffic impact study is to provide City staff and policy makers with data they can use to make an informed decision regarding the potential traffic impacts of a proposed project, and any associated improvements that would be required to mitigate these impacts to a level of insignificance and reduce adverse effects to an acceptable level as defined by the City's General Plan or other policies. Vehicular traffic operational effects are typically evaluated by determining the number of new trips that the proposed use would be expected to generate, distributing these trips to the surrounding street system based on existing travel patterns or anticipated travel patterns specific to the proposed project, then analyzing the effect the new traffic would be expected to have on critical intersections or roadway segments. While the traffic operational analysis is required by the City and used to confirm consistency with General Plan policies, it is not used for CEQA purposes, consistent with updates to the CEQA guidelines adopted by the State of California. CEQA transportation impacts are assessed through analysis of vehicle miles traveled (VMT), with evaluation of non-auto modes including access for pedestrians, bicyclists, and to transit, and circulation safety.

## Project Profile

The proposed project includes the development of 142 affordable apartments on a site that is currently vacant, as shown in Figure 1. The project would include a driveway onto Old Stony Point Road as well as a driveway onto Hearn Avenue near the eastern project boundary.

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## Transportation Setting

## Operational Analysis

## Study Area and Periods

The study area consists of the sections of Hearn Avenue and Old Stony Point Road fronting the project site as well as the following intersections.

1. Stony Point Road/Northpoint Parkway
2. Stony Point Road/Hearn Avenue
3. Hearn Avenue/Old Stony Point Road
4. Hearn Avenue/Burbank Avenue
5. Hearn Avenue/Dutton Meadow

Operating conditions during the a.m. and p.m. peak periods were evaluated to capture the highest potential impacts for the proposed project as well as the highest volumes on the local transportation network. The morning peak hour occurs between 7:00 and 9:00 a.m. and reflects conditions during the home to work or school commute, while the p.m. peak hour occurs between 4:00 and 6:00 p.m. and typically reflects the highest level of congestion during the homeward bound commute.

## Study Intersections

Stony Point Road/Northpoint Parkway is a signalized tee intersection with protected-permitted left-turn phasing including flashing yellow arrow (FYA) signal heads on the northbound approach. There are crosswalks on the north and west legs of the intersection.

Stony Point Road/Hearn Avenue is a signalized intersection with protected left-turn phasing on all approaches, and a right-turn overlap phase on the westbound approach. Crosswalks are provided on all legs.

Stony Point Road/Old Stony Point Road is a three-legged unsignalized intersection that is stop-controlled on the southbound Old Stony Point Road approach. A left-turn lane is provided on the eastbound Hearn Avenue approach, and the east leg has a two-way left-turn lane. A marked crosswalk with rapid rectangular flashing beacon (RRFB) pedestrian crossing lights is located on the east intersection leg.

Hearn Avenue/Burbank Avenue is an unsignalized intersection that is stop-controlled on the northbound Southwest Community Park access and the southbound Burbank Avenue approach. Left-turn lanes are provided on the eastbound and westbound Hearn Avenue approaches and the east leg has a marked crosswalk.

Hearn Avenue/Dutton Meadow is a three-legged signalized intersection. The westbound left-turn has protected phasing, along with overlap phasing for the northbound right-turn movement. The west leg has a crosswalk and curb ramps.

The locations of the study intersections and the existing lane configurations and controls are shown in Figure 1.

## Collision History

The collision history for the study area was reviewed to determine any trends or patterns that may indicate a safety issue. Collision rates were calculated based on records available from the California Highway Patrol as published
in their Statewide Integrated Traffic Records System (SWITRS) reports. The most current five-year period available is November 1, 2014 through October 31, 2019.

As presented in Table 1, the calculated collision rates for the study intersections were compared to average collision rates for similar facilities statewide, as indicated in 2016 Collision Data on California State Highways, California Department of Transportation (Caltrans). These average rates statewide are for intersections in the same environment (urban), with the same number of approaches (three or four), and the same controls (two-way stop or signalized). Collision rates for three of the five study intersections were above the statewide average so were further reviewed. The collision rate calculations are provided in Appendix A.

Table 1 - Collision Rates for the Study Intersections

| Study Intersection | Number of <br> Collisions <br> $(\mathbf{2 0 1 4 - 2 0 1 9 )}$ | Calculated <br> Collision Rate <br> (c/mve) | Statewide Average <br> Collision Rate <br> (c/mve) |
| :--- | :---: | :---: | :---: |
| 1. Stony Point Rd/Northpoint Pkwy | 15 | $\mathbf{0 . 3 5}$ | 0.28 |
| 2. Stony Point Rd/Hearn Ave | 15 | 0.38 | 0.43 |
| 3. Hearn Ave/Old Stony Point Rd | 2 | 0.12 | 0.14 |
| 4. Hearn Ave/Burbank Ave | 6 | $\mathbf{0 . 2 5}$ | 0.23 |
| 5. Hearn Ave/Dutton Meadow | 9 | $\mathbf{0 . 3 3}$ | 0.28 |

Note: $\quad c / m v e=$ collisions per million vehicles entering; Bold text $=$ higher collision rate than statewide average

The collision rate at Stony Point Road/Northpoint Parkway is higher than the statewide average, with 13 of the 15 reported collisions being either rear-end, hit object or right-angle collisions. Rear-end crashes are common at signalized intersections during congested conditions. Right-angle collisions can result from right-of-way violations. It is noted that this intersection was within a construction zone for a long period during the Stony Point Road widening project; 11 of the 15 crashes occurred prior to completion of the Stony Point Road widening, and collision frequency has decreased since that time.

The predominant crash type at Hearn Avenue/Burbank Avenue was right-angle collisions. Three of the five rightangle crashes involved vehicles entering Hearn Avenue from either Burbank Avenue or the Southwest Community Park and two involved vehicles turning into Burbank Avenue or the Park from Hearn Avenue. It is understood that the City has added signalization of this intersection to the Capital Improvement Program (CIP), and such an installation would reduce the frequency of these types of crashes.

Review of the collisions reported at Hearn Avenue/Dutton Meadow indicates that 7 of the 10 collisions were rearend collisions, which occurred on the westbound and eastbound approaches to the intersection. The most common primary collision factor cited was unsafe speed. An increased enforcement presence may help to reduce the frequency of these types of collisions.

## Alternative Modes

## Pedestrian Facilities

Pedestrian facilities include sidewalks, crosswalks, pedestrian signal phases, curb ramps, curb extensions, and various streetscape amenities such as lighting, benches, etc. In general, a network of sidewalks, crosswalks, pedestrian signals, and curb ramps provide access for pedestrians in the vicinity of the proposed project site where property has been developed; however, sidewalk gaps can be found along streets near the project site.

- Hearn Avenue - Several sections of sidewalk are provided from Stony Point Road to Dutton Meadow, but there are large gaps in sidewalk coverage on both sides of Hearn Avenue. In these areas with no sidewalk, pedestrians walk on paved shoulders or cross Hearn Avenue to access the segments of Hearn Avenue that include a sidewalk. Lighting is provided by overhead lights, mainly on the north side of the street.
- Old Stony Point Road - The east side of this minor street currently has a combination of sidewalks and asphalt paths separated from vehicle lanes by an asphalt berm. The sidewalks and paths connect to existing facilities on Hearn Avenue and Stony Point Road.


## Bicycle Facilities

The Highway Design Manual, Caltrans, 2017, classifies bikeways into four categories:

- Class I Multi-Use Path - a completely separated right-of-way for the exclusive use of bicycles and pedestrians with cross flows of motorized traffic minimized.
- Class II Bike Lane - a striped and signed lane for one-way bike travel on a street or highway.
- Class III Bike Route - signing only for shared use with motor vehicles within the same travel lane on a street or highway.
- Class IV Bikeway - also known as a separated bikeway, a Class IV Bikeway is for the exclusive use of bicycles and includes a separation between the bikeway and the motor vehicle traffic lane. The separation may include, but is not limited to, grade separation, flexible posts, inflexible physical barriers, or on-street parking.

In the project area, Class II bike lanes exist on Hearn Avenue between Stony Point Road and Dutton Meadow, extending eastward to the SMART multi-use pathway. Continuous bicycle lanes also exist on Stony Point Road within the study area, extending northward over four miles through much of western Santa Rosa. Bicyclists ride in the roadway and/or on sidewalks along all other streets within the project study area. Table 2 summarizes the existing and planned bicycle facilities in the project vicinity, as contained in the City of Santa Rosa Bicycle \& Pedestrian Master Plan Update 2018.

Table 2 - Bicycle Facility Summary

| Status |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Facility | Class | Length <br> (miles) | Begin Point | End Point |
| Existing <br> Hearn Ave | II | 1.15 | Stony Point Rd | Whitewood Dr |
| Stony Point Rd-Marlow Rd | II | 4.80 | Piner Rd | Bellevue Ave |
| Planned |  |  |  |  |
| Burbank Ave | II | 1.00 | Roundelay Ln | Hearn Ave |
| Dutton Meadow | II | 0.86 | Hearn Ave | Bellevue Ave |
| Northpoint Pkwy | IV | 0.33 | Stony Point Rd | Burbank Ave |

Source: City of Santa Rosa Bicycle \& Pedestrian Master Plan Update 2018, City of Santa Rosa, 2018

## Transit Facilities

Santa Rosa CityBus provides fixed route bus service in Santa Rosa. Routes 12 and 15 serve the study area seven days a week. Route 15 stops on Stony Point Road just north of Pearblossom Drive near the northern terminus of Old Stony Point Road; the northbound bus stop is approximately 450 feet from the proposed project's driveway on Old Stony Point Road, and the southbound bus stop is approximately 800 feet from the project driveway. Route 15 also stops at the intersection of Hearn Avenue/Arrowhead Drive, approximately 650 feet southeast of the
project's Old Stony Point Road driveway. Routes 12 and 15 stop at Southwest Community Park, which is approximately 120 feet south of the intersection of Hearn Avenue/ Burbank Avenue, and roughly one-half mile east of the project site. The bus stops on Hearn Avenue and Southwest Community Park are accessible from the project site via Old Stony Point Road and existing sidewalks on the south side of Hearn Avenue.

Route 12 operates Monday through Friday with approximately one-hour headways between $6: 15$ a.m. and 7:15 p.m. Weekend service operates with approximately one-hour headways between 10:15 a.m. and 4:15 p.m. Route 15 operates Monday through Friday with approximately one-hour headways between 6:20 a.m. and 7:20 p.m. Weekend service operates with approximately one-hour headways between 10:20 a.m. and 4:20 p.m. These schedules are indicative of pre COVID-19 conditions but are anticipated to resume in the future.

Two to three bicycles can be carried on most CityBus buses. Bike rack space is on a first-come, first-served basis.
Paratransit, also known as dial-a-ride, or door-to-door service, is available for those who are unable to independently use the transit system due to a physical or mental disability. CityBus paratransit is contracted out to MV Transportation and is designed to serve the needs of individuals with disabilities within three-quarters (3/4) of a mile from existing CityBus routes. Paratransit service is available seven days a week, but rides must be scheduled one day in advance.

## Capacity Analysis

## Intersection Level of Service Methodologies

Level of Service (LOS) is used to rank traffic operation on various types of facilities based on traffic volumes and roadway capacity using a series of letter designations ranging from A to F. Generally, Level of Service A represents free flow conditions and Level of Service F represents forced flow or breakdown conditions. A unit of measure that indicates a level of delay generally accompanies the LOS designation.

The study intersections were analyzed using methodologies published in the Highway Capacity Manual (HCM), Transportation Research Board, $6^{\text {th }}$ Edition, 2018. This source contains methodologies for various types of intersection control, all of which are related to a measurement of delay in average number of seconds per vehicle.

The Levels of Service for the intersections with side street stop controls, or those which are unsignalized and have one or two approaches stop controlled, were analyzed using the "Two-Way Stop-Controlled" intersection capacity method from the HCM. This methodology determines a level of service for each minor turning movement by estimating the level of average delay in seconds per vehicle. Results are presented for individual movements together with the weighted overall average delay for the intersection.

The study intersections that are controlled by a traffic signal were evaluated using the signalized methodology from the HCM. This methodology is based on factors including traffic volumes, green time for each movement, phasing, whether the signals are coordinated or not, truck traffic, and pedestrian activity. Average stopped delay per vehicle in seconds is used as the basis for evaluation in this LOS methodology. For purposes of this study, delays were calculated using signal timing obtained from City of Santa Rosa.

The ranges of delay associated with the various levels of service are indicated in Table 3.

| LOS | Two-Way Stop-Controlled | Signalized |
| :---: | :---: | :---: |
| A | Delay of 0 to 10 seconds. Gaps in traffic are readily available for drivers exiting the minor street. | Delay of 0 to 10 seconds. Most vehicles arrive during the green phase, so do not stop at all. |
| B | Delay of 10 to 15 seconds. Gaps in traffic are somewhat less readily available than with LOS A, but no queuing occurs on the minor street. | Delay of 10 to 20 seconds. More vehicles stop than with LOS A, but many drivers still do not have to stop. |
| C | Delay of 15 to 25 seconds. Acceptable gaps in traffic are less frequent, and drivers may approach while another vehicle is already waiting to exit the side street. | Delay of 20 to 35 seconds. The number of vehicles stopping is significant, although many still pass through without stopping. |
| D | Delay of 25 to 35 seconds. There are fewer acceptable gaps in traffic, and drivers may enter a queue of one or two vehicles on the side street. | Delay of 35 to 55 seconds. The influence of congestion is noticeable, and most vehicles have to stop. |
| E | Delay of 35 to 50 seconds. Few acceptable gaps in traffic are available, and longer queues may form on the side street. | Delay of 55 to 80 seconds. Most, if not all, vehicles must stop, and drivers consider the delay excessive. |
| F | Delay of more than 50 seconds. Drivers may wait for long periods before there is an acceptable gap in traffic for exiting the side streets, creating long queues. | Delay of more than 80 seconds. Vehicles may wait through more than one cycle to clear the intersection. |

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## Traffic Operation Standards

The City of Santa Rosa establishes measures of effectiveness for traffic operational analyses in Guidance for the Preparation of Traffic Operational Analysis, July 2019. This document refers to and builds upon the following policies included in section 5.8 (Transportation Goals \& Policy) of the City of Santa Rosa General Plan.

T-D-1 Maintain a Level of Service (LOS) D or better along all major corridors. Exceptions to meeting the standard include:

- Within downtown;
- Where attainment would result in significant degradation;
- Where topography or impacts makes the improvement impossible; or
- Where attainment would ensure loss of an area's unique character.

The LOS is to be calculated using the average traffic demand over the highest 60-minute period.
Traffic Engineering Division will require a level of service evaluation of arterial and collector corridors if deemed necessary.

T-D-2 Monitor level of service at intersections to assure that improvements or alterations to improve corridor level of service do not cause severe impacts at any single intersection.

General interpretation of Policy T-D-2. The impact to an intersection is considered adverse if the project related and/or future trips result in:

1. The level of service (LOS) at an intersection degrading from LOS D or better to LOS E or $F, O R$
2. An increase in average vehicle delay of greater than 5 seconds at a signalized intersection where the current LOS is either LOS E or F .
3. Queuing impacts based on a comparative analysis between the design queue length and the available queue storage capacity. Impacts include, but are not limited to, spillback queue at project access locations (both ingress and egress), turn lanes at intersections, lane drops, spill back that impacts upstream intersections or interchange ramps.
4. Exceptions may be granted under the following conditions:
a. Within downtown,
b. Where attainment would result in significant degradation,
c. Where topography or impacts makes the improvement impossible; or
d. Where attainment would ensure loss of an area's unique character.

T-C-3 Implement traffic calming techniques on streets subject to high speed and/or cut-through traffic, in order to improve neighborhood livability, Techniques Include:

- Narrow Streets
- On-street parking
- Choker or diverters
- Decorative crosswalks
- Planted islands

General interpretation of Policy T-C-3. An impact is considered adverse if the project has the potential to alter community character by significantly increasing cut-through traffic, unexpected vehicle maneuvers or commercial vehicle trips in a residential area.

T-H-3 Require new development to provide transit improvements, where a rough proportionality to demand from the project is established. Transit improvements may include:

- Direct and paved pedestrian access to transit stops
- Bus turnouts and shelters
- Lane width to accommodate buses.

General interpretation of Policy T-H-3. An impact is considered adverse if the project has the potential to disrupt existing transit operations or establishes transit facilities and equipment such that it creates a sight distance deficiency or vehicle conflict point.

## T-J Provide attractive and safe streets for pedestrian and bicyclists.

General interpretation of Policy T-J. An impact is considered adverse if the project generates 20 pedestrians in any single hour at an unsignalized intersection, mid-block crossing or where no crossing has been established.

An impact is further considered significant if the project interrupts existing or proposed pedestrian, bicycle and transit facilities, path or travel, direct access resulting in excessive rerouting or creates a vehicle conflict condition which affects the safety of other roadway users.

## Use of LOS E or F at Unsignalized Intersections

On sections of certain arterial streets, it is typical to have all side streets operating at LOS E or F with long traffic delays, even where side street volumes are very low. In fact, it may be operationally, physically, and/or financially infeasible to provide mitigation which would allow LOS D or better operation from all side streets during peak hours. The most typical mitigation measure used to improve operation for the side street is a traffic signal, and it is both operationally and financially undesirable to provide a traffic signal at every intersection along most street segments. For these reasons, mitigation measures were considered when only when LOS F conditions were projected for minor movements at unsignalized intersections.

## Existing Conditions

The Existing Conditions scenario provides an evaluation of current operation based on existing traffic volumes during the a.m. and p.m. peak periods. This condition does not include project-generated traffic volumes.

Because the COVID-19 pandemic has had a substantial effect on traffic patterns, the existing volumes applied in this analysis have been adjusted to reflect non-pandemic conditions using a combination of new and previously obtained counts. Traffic counts at the intersections of Stony Point Road/Northpoint Parkway, Stony Point Road/Hearn Avenue, and Hearn Avenue/Dutton Meadow from 2017 and 2018 were factored by a growth rate of one percent per year to reflect current conditions. Counts obtained in September 2019 at Hearn Avenue/Burbank Avenue were directly applied. New counts were obtained at the Hearn Avenue/Old Stony Point Road intersection in December 2020. Growth factors were applied to these volumes based on a comparison of COVID versus nonCOVID volumes on the segment of Hearn Avenue between Stony Point Road and Old Stony Point Road, and in consideration of the traffic volumes that would typically be expected on Old Stony Point Road based on the approximately 70 apartments and five single-family homes that currently rely on the street for access. This approach was discussed with and approved by the City's Traffic Engineer.

Under existing conditions, all study intersections are operating acceptably overall. Although the intersection of Hearn Avenue/Burbank Avenue is operating acceptably at LOS A overall, the City is aware of the high delays experienced on the southbound approach and has plans to signalize the intersection, as detailed in the 2016

Roseland Area/Sebastopol Road Specific Plan. The installation of a signal would be expected to reduce the delays on the southbound approach to an acceptable Level of Service.

The existing traffic volumes are shown in Figure 2. A summary of the intersection Level of Service calculations is contained in Table 4, and copies of the calculations are provided in Appendix B.

Table 4 - Existing Peak Hour Intersection Levels of Service

| Study Intersection <br> Approach |  | AM Peak |  | PM Peak |  |
| :--- | :--- | :---: | :---: | :---: | :---: |
| 1. | Stony Point Rd/Northpoint Pkwy | LOS | Delay | LOS |  |
| 2. | Stony Point Rd/Hearn Ave | 8.4 | A | 18.9 | B |
| 3. | Hearn Ave/Old Stony Point Rd | 0.4 | D | 29.1 | C |
|  | Southbound (Old Stony Point Rd) Approach | 11.6 | A | 0.9 | A |
| 4. | Hearn Ave/Burbank Ave | 8.6 | A | 6.9 | A |
|  | Southbound (Burbank Ave) Approach | 62.4 | F | 49.8 | E |
| 5. | Hearn Ave/Dutton Meadow | 15.8 | B | 9.1 | A |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics

## Baseline Conditions

Baseline (Existing plus Approved) operating conditions were assessed with traffic from approved projects in and near the study area added to the Existing volumes. As directed by staff, the following ten projects contained in the Citywide Summary of Pending Development report published by the City in May 2020 were included in the evaluation of Baseline Conditions. Unless stated otherwise, the same trip generation and distribution assumptions used in the traffic studies for the various projects, where available, were used in this analysis.

Southwest Estates is an approved 60 single-family residence development at 533 Bellevue Avenue. As contained in the Traffic Impact Study for the Southwest Estates, W-Trans, August 2008, the project is expected to generate a total of 566 trips per day, including 44 trips during the a.m. peak hour and 59 trips during the p.m. peak hour.

Burbank Avenue Subdivision includes an approved 64 apartments and 74 single-family dwellings at 1400 Burbank Avenue. As contained in the Traffic Impact Study for the Burbank Avenue Subdivision, W-Trans, December 2019, the project is expected to generate a total of 1,158 trips per day, including 83 trips during the a.m. peak hour and 108 trips during the p.m. peak hour.

Somerset Place has been approved with 32 single-family dwelling units at 2786 Dutton Meadow. The trip generation for this project (as well as others with no available traffic studies) was calculated using standard rates published by the Institute of Transportation Engineers (ITE) in the Trip Generation Manual, $10^{\text {th }}$ Edition. The project is expected to generate 302 daily trips on average, with 24 trips during the morning peak period and 32 trips during the evening peak period.

Meadowood Ranch is an approved single-family residential development with 78 units at 2853 Dutton Meadow. The project is expected to generate 736 daily trips on average, with 58 trips during the morning peak period and 77 trips during the evening peak period.


## Traffic Impact Study for Stony Oaks Apartments

Figure 2 - Existing Traffic Volumes

Bellevue Ranch 7 is an approved 30-unit development of single-family dwellings at 2903 Dutton Meadow. The project is expected to generate 283 daily trips on average, with 22 trips during the morning peak period and 30 trips during the evening peak period.

Lantana Place is an approved 48 single-family dwelling development at 2979 Dutton Meadow. The project is expected to generate 453 daily trips on average, with 36 trips during the morning peak period and 48 trips during the evening peak period.

Air Center East Phase 2 includes 133 single-family dwellings approved for 1301 Ludwig Avenue. The project is expected to generate 1,256 daily trips on average, with 98 trips during the morning peak period and 132 trips during the evening peak period.

Stony Village North has been approved with 47 single-family dwellings at 2729 Stony Point Road. As contained in the Traffic Impact Study for the Stony Village North Project, W-Trans, January 2016, the project is expected to generate a total of 436 trips per day, including 34 trips during the a.m. peak hour and 45 trips during the p.m. peak hour.

Grove Village is an approved 157 single-family dwelling project at 2880 Stony Point Road. The project is expected to generate 1,482 daily trips on average, with 116 trips during the morning peak period and 155 trips during the evening peak period.

Roseland Accelerated Middle School as proposed would relocate an existing 300-student middle school campus to the Roseland Creek Elementary School site on Burbank Avenue. The project is expected to generate 567 trips per day, including 189 trips during the morning peak hour and 105 trips during the evening peak hour.

Upon adding trips from the approved projects to Existing volumes, the study intersections are expected to continue operating at acceptable service levels overall. The southbound approach at Hearn Avenue/Burbank Avenue would experience increased delays and LOS F operation, and the "peak hour" signal warrant would be met (see additional signal warrant discussion under Access and Circulation). These results are summarized in Table 5 and Baseline volumes are shown in Figure 3.

## Table 5 - Baseline Peak Hour Intersection Levels of Service

| Study Intersection <br> Approach |  | AM Peak |  | PM Peak |  |
| :--- | :--- | :---: | :---: | :---: | :---: |
|  | Delay | LOS | Delay | LOS |  |
| 1. | Stony Point Rd/Northpoint Pkwy | 8.4 | A | 19.7 | B |
| 2. | Stony Point Rd/Hearn Ave | 42.2 | D | 35.5 | D |
| 3. | Hearn Ave/Old Stony Point Rd | 0.4 | A | 0.8 | A |
|  | Southbound (Old Stony Point Rd) Approach | 12.1 | B | 13.5 | B |
| 4. | Hearn Ave/Burbank Ave | 37.3 | D | 23.1 | C |
|  | Southbound (Burbank Ave) Approach | 244.5 | F | 161.7 | F |
| 5. | Hearn Ave/Dutton Meadow | 20.7 | C | 10.7 | B |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics


## Traffic Impact Study for Stony Oaks Apartments

Figure 3 - Baseline Traffic Volumes

## Project Description

The proposed project includes the development of 142 affordable apartments on a site that is currently vacant. The project would include driveways onto Old Stony Point Road as well as Hearn Avenue near the eastern project boundary. The proposed project site plan is shown in Figure 4.

## Trip Generation

The anticipated trip generation for the proposed project was estimated using standard rates published by the Institute of Transportation Engineers (ITE) in Trip Generation Manual, $10^{\text {th }}$ Edition, 2017 for "Multi-Family Housing (Mid-Rise)" (Land Use \#221). Based on application of these rates, the proposed project is expected to generate an average of 772 trips per day, including 51 a.m. peak hour trips and 62 trips during the p.m. peak hour. These results are summarized in Table 6.

## Table 6 - Trip Generation Summary

| Land Use | Units | Daily |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Rate | Trips | Rate | Trips | In | Out | Rate | Trips | In | Out |
| Multi-Family Housing (Mid-Rise) | 142 du | 5.44 | 772 | 0.36 | 51 | 13 | 38 | 0.44 | 62 | 38 | 24 |

Note: $\quad d u=$ dwelling unit

## Trip Distribution

The pattern used to allocate new project trips to the street network was determined by reviewing existing turning movements at the study intersections. Trips routed from and to the west were assumed to be equally split between the project's driveways on Old Stony Point Road and Hearn Avenue. All trips routed from and to the east were assigned to the project's Hearn Avenue driveway. The applied distribution assumptions and resulting trips are shown in Table 7.

Table 7 - Trip Distribution Assumptions

| Route | Percent | AM Trips | PM Trips |
| :--- | :---: | :---: | :---: |
| From/to the north via Stony Point Rd | $45 \%$ | 23 | 28 |
| From/to the east via Hearn Ave | $40 \%$ | 20 | 25 |
| From/to the south via Stony Point Rd | $15 \%$ | 8 | 9 |
| TOTAL | $\mathbf{1 0 0 \%}$ | $\mathbf{5 1}$ | $\mathbf{6 2}$ |

## Existing plus Project Conditions

Upon the addition of project-related traffic to the Existing volumes, the study intersections are expected to continue operating acceptably overall. Operation on the southbound approach to Hearn Avenue/Burbank Avenue would deteriorate from LOS E to LOS F, though the increase due to the project would be less than five seconds. The project is anticipated to increase overall average delay at the Hearn Avenue/Burbank Avenue intersection by 0.4 to 0.5 seconds, though the "peak hour" warrant for signalization would be unmet (see additional signal warrant discussion in Access and Circulation). Project traffic volumes are shown in Figure 5. These results are summarized in Table 8.


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## Traffic Impact Study for Stony Oaks Apartments

Figure 5 - Project Traffic Volumes

Table 8 - Existing and Existing plus Project Peak Hour Intersection Levels of Service

| Study Intersection Approach | Existing Conditions |  |  |  | Existing plus Project |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM Peak |  | PM Peak |  | AM Peak |  | PM Peak |  |
|  | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| 1. Stony Point Rd/Northpoint Pkwy | 8.4 | A | 18.9 | B | 8.4 | A | 19.0 | B |
| 2. Stony Point Rd/Hearn Ave | 39.7 | D | 29.1 | C | 39.8 | D | 29.3 | C |
| 3. Hearn Ave/Old Stony Point Rd | 0.4 | A | 0.9 | A | 0.6 | A | 1.0 | A |
| SB (Old Stony Point Rd) Approach | 11.6 | B | 12.8 | B | 11.5 | B | 13.0 | B |
| 4. Hearn Ave/Burbank Ave | 8.6 | A | 6.9 | A | 9.1 | $B$ | 7.3 | A |
| SB (Burbank Ave) Approach | 62.4 | $F$ | 49.8 | E | 67.1 | $F$ | 54.1 | $F$ |
| 5. Hearn Ave/Dutton Meadow | 15.8 | B | 9.1 | A | 16.2 | B | 9.2 | A |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics; SB = Southbound

Finding - The study intersections are expected to continue operating acceptably overall at the same levels of service upon the addition of project-generated traffic. Although the southbound approach to Hearn Avenue/Burbank Avenue is expected to operate at LOS F, the project's impact would be considered less-thansignificant as the intersection would be expected to continue operating acceptably overall and the peak hour signalization warrant would be unmet.

## Baseline plus Project Conditions

With project-related traffic added to Baseline volumes, the study intersections are expected to continue operating acceptably and the southbound approach at Hearn Avenue/Burbank Avenue would continue to operate at LOS F until the planned traffic signal is installed. Under Baseline plus Project conditions, the project is anticipated to increase overall delay at the Hearn Avenue/Burbank Avenue intersection by 1.7 to 2.2 seconds as compared to Baseline conditions without the project. Under both Baseline and Baseline plus Project conditions, the "peak hour" signal warrant would be met. These results are summarized in Table 9.

Table 9 - Baseline and Baseline plus Project Peak Hour Intersection Levels of Service

| Study Intersection | Baseline Conditions |  |  |  | Baseline plus Project |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | AM Peak | PM Peak | AM Peak |  | PM Peak |  |  |  |

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in italics; SB = Southbound

Finding - The study intersections are expected to continue operating acceptably overall at the same Levels of Service upon the addition of project-generated traffic to Baseline conditions as without it. Although the southbound approach to Hearn Avenue/Burbank Avenue is expected to operate at LOS F, the project's impact would be considered acceptable as the intersection would be expected to continue operating acceptably overall, the peak hour signal warrant would be met both without and with the project, and the project would be expected to increase overall delays by less than five seconds.

## Vehicle Miles Traveled

## Background and Applied Thresholds

Senate Bill (SB) 743 established a change in the metric to be applied for determining traffic impacts associated with development projects. Rather than the delay-based criteria associated with a Level of Service analysis, the increase in Vehicle Miles Traveled (VMT) as a result of a project is now the basis for determining transportation impacts. The City of Santa Rosa has established parameters for VMT analyses in the Vehicles Miles Traveled Guidelines Final Draft, June 2020. The City's parameters are consistent with guidance provided in the publication Transportation Impacts (SB 743) CEQA Guidelines Update and Technical Advisory, California Governor's Office of Planning and Research (OPR), 2018. Both documents indicate that a residential project generating vehicle travel that is 15 or more percent below the existing countywide residential VMT per capita may indicate a less than significant VMT impact.

## VMT Analysis

Based on data from the version of the Sonoma County Transportation Authority (SCTA) travel demand model released in October 2020, the County of Sonoma has a baseline average residential VMT of 16.53 miles per capita. A residential project generating a VMT that is 15 percent or more below this value, or 14.05 miles per capita or less, would have a less-than-significant VMT impact. The SCTA model includes traffic analysis zones (TAZ) covering geographic areas throughout Sonoma County. The project site is located within TAZ 500, which has a baseline VMT per capita of 13.01 miles. Because this per capita VMT ratio is below the significance threshold of 14.05 miles, the project would be considered to have a less-than-significant VMT impact. A map excerpt from the SCTA travel demand model showing the residential VMT per capita for TAZs in the project vicinity is included in Appendix C.

The City's VMT guidelines and OPR Technical Advisory also include screening criteria which identify certain types of projects that may be presumed to have a less than significant VMT impact, including developments comprised of 100 percent affordable housing. The proposed Stony Oaks project would qualify for this screening criteria in addition to falling below the VMT per capita significance threshold.

Finding - The project would have a less-than-significant impact on vehicle miles traveled.

## Alternative Modes

## Pedestrian Facilities

The site would include an onsite network of pedestrian sidewalks and paths. Given that the site is an infill location within existing neighborhoods and near school, recreation, and employment uses, it is reasonable to assume that some project residents would want to walk and/or use transit to reach destinations beyond the site. As proposed, the project would include a sidewalk along its entire frontage of Old Stony Point Road, replacing the current asphalt path and dike and connecting to the existing pedestrian network to the north and south. From this pedestrian connection on Old Stony Point Road, residents would be able to access nearby bus stops on Stony Point Road, Hearn Avenue, and at Southwest Community Park. Enhanced pedestrian crossings including RRFB warning devices are already in place near the transit stops on both Stony Point Road and Hearn Avenue.

The project would also provide a short segment of sidewalk on its limited Hearn Avenue frontage. Currently, the north side of Hearn Avenue to the east and west has sidewalk gaps that are anticipated to be filled over time as adjacent properties develop or redevelop. Until such time as those sidewalks are constructed in the future, residents of the proposed project would still have continuous access to the surrounding pedestrian network and transit facilities via existing sidewalks on Old Stony Point Road and the south side of Hearn Avenue. The City has indicated that pedestrian access at the site's Hearn Avenue driveway will need to be restricted until sidewalk gaps are filled in the future.

Finding - Pedestrian facilities serving the project site would be adequate upon the completion of the proposed frontage improvements.

## Bicycle Facilities

The existing Class II bike lanes on Hearn Avenue along with planned future bicycle facilities in the vicinity would provide adequate access for bicyclists. Residents of the proposed development would be able to use the existing bike lanes on Hearn Avenue to connect to many of the primary bicycle facilities in the City.

Finding - Bicycle facilities serving the project site are adequate.

## Transit

Existing transit routes are adequate to accommodate project-generated transit trips. Bus stops serving two CityBus routes are within a convenient walking distance of the site and accessible by the existing pedestrian network.

Finding - Transit facilities serving the project site are adequate.

## Access and Circulation

## Site Access

The project would include two driveways providing primary access to the proposed apartments, one on Old Stony Point Road at the site's western property boundary and one on Hearn Avenue near the site's eastern property boundary. Old Stony Point Road is a low-volume local street that terminates 300 feet north of the project site; given the nature of the street no potential conflicts would be created by the proposed driveway. The project driveway on Hearn Avenue would be located on a segment of the corridor that has existing two-way left-turn lanes, and the south side of Hearn Avenue near the project site includes single-family homes that generate very low volumes of turning traffic. The two-way left-turn lane will provide space for eastbound drivers to turn left into the site, and for outbound drivers to make left-turns in two separate movements during busier periods. The driveway is anticipated to function acceptably.

## Sight Distance

Sight distances along Old Stony Point Road and Hearn Avenue at the project driveways were evaluated based on sight distance criteria contained in the Highway Design Manual published by Caltrans. The recommended sight distance for driveway approaches is based on stopping sight distance and uses the approach travel speed as the basis for determining the recommended sight distance.

For Old Stony Point Road, which has a speed of 25 mph , the minimum stopping sight distance is 150 feet. The minimum stopping sight distance for Hearn Avenue, which has a posted speed limit of 30 mph , is 200 feet. Available sight lines were field measured and exceed 200 feet at both driveways, which meets the sight distance requirements.

Finding - Based on field observations and review of the project site plan, the project's proposed driveways are anticipated to operate acceptably, with adequate sight distances along Old Stony Point Road and Hearn Avenue.

Recommendation - To maintain clear lines of sight from the project driveways it is recommended that any landscaping be low-profile and that trees be set back outside the vision triangle.

## Emergency Access

Emergency response vehicles could access the site via the main access point on Old Stony Point Road as well as the Hearn Avenue driveway. The AutoTURN application of AutoCAD was used to evaluate the adequacy of access for emergency vehicles based on the project site plan. As designed, there would be no anticipated issues with fire truck access. An exhibit showing the expected travel paths on the site plan is provided in Appendix D.

Finding - Emergency access is expected to function acceptably.

## Onsite Circulation

The site consists of a group of apartment buildings surrounded by drive aisles that loop around the buildings and include perpendicular parking spaces. All drive aisles connect internally, allowing access to both Old Stony Point Road and Hearn Avenue.

Finding - Onsite circulation is anticipated to function acceptably.

## Traffic Signal Warrants

Because the intersection of Hearn Avenue/Burbank Avenue has LOS F operation on the minor stop-controlled approach in all project scenarios, a signal warrants analysis was performed. Chapter 4C of the California Manual on Uniform Traffic Control Devices (CA-MUTCD) provides guidance on when a traffic signal should be considered. There are nine different warrants, or criteria, but for the purposes of this study, Warrant 3 (the peak hour warrant) was evaluated. Warrant 3 determines the need for traffic control based on the highest volume hour of the day and was used as an initial indication of traffic control needs. The use of this signal warrant is common practice for planning studies.

Warrant 3: Under the Peak Hour Warrant the need for a traffic control signal shall be considered if an engineering study finds that the criteria in either of the following two categories are met:
A. If all three of the following conditions exist for the same one hour (any four consecutive 15-minute periods) of an average day:

1. The total stopped time delay experienced by the traffic on one minor-street approach (one direction only) controlled by a STOP sign equals or exceeds: four vehicle-hours for a one-lane approach; or five vehicle-hours for a two-lane approach, and
2. The volume on the same minor-street approach (one direction only) equals or exceeds 100 vehicles per hour for one moving lane of traffic or 150 vehicles per hour for two moving lanes, and
3. The total entering volume serviced during the hour equals or exceeds 650 vehicles per hour for intersections with three approaches or 800 vehicles per hour for intersections with four or more approaches.
B. The plotted point representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor-street approach (one direction only) for one hour (any four consecutive 15 -minute periods) of an average day falls above the applicable curve in Figure 4C-3 for the existing combination of approach lanes.

Despite LOS F operation on the southbound approach of Hearn Avenue/Burbank Avenue, the signal warrant would be unmet under both Existing and Existing plus Project conditions. Under Baseline volumes both without and with the project, the signal warrant would be met. Copies of the Signal Warrant Spreadsheets are provided in Appendix E.

As noted in the operational analysis, signalization of the Hearn Avenue/Burbank Avenue intersection was identified as a planned future improvement in the Roseland Area/Sebastopol Road Specific Plan and its EIR and has since been added to the City's Capital Improvement Program. The signal is to be funded by development projects in the area. Because the project would contribute to the need for these improvements, the City has indicated that the project should pay a proportional share fee toward the cost of construction, with the share determined by the project's contribution to added delays on the critical southbound approach during the worst-case a.m. peak hour.

Based on the operational analysis, the project would be responsible for 9.3 percent of the projected increases in delay occurring between Existing and Baseline plus Project conditions. As contained in the Infrastructure Report for Roseland Area/Sebastopol Road Specific Plan and Roseland Area Annexation, Michael Baker International, 2016, signalization of the Hearn Avenue/Burbank Avenue intersection is estimated to have a total cost of $\$ 320,000$ ( $\$ 200,000$ for construction and $\$ 120,000$ for soft costs). The applicant's proportionate share of this fee would therefore be $\$ 29,760$. A summary of the proportionate share calculation is provided in Appendix F.

Finding - The Peak Hour Volume warrant would be met at the intersection of Hearn Avenue/Burbank Avenue under both Baseline and Baseline plus Project Conditions. The need for signalization was identified in the Roseland Area/Sebastopol Road Specific Plan and the project has been added to the City's Capital Improvement Program.

Recommendation - As directed by the City, the applicant should contribute a proportional share of funds for the signalization of the intersection of Hearn Avenue/Burbank Avenue. The project would be responsible for 9.3 percent of the cost, or $\$ 29,760$.

## Parking

Parking was evaluated to determine if the proposed parking supply would be adequate to satisfy City and State requirements. Per the project site plan, a total of 185 parking spaces will be provided on-site, including 13 ADAaccessible spaces. Section 20-36.040 of the Santa Rosa City Code requires multifamily affordable housing projects to provide one parking space per one-bedroom unit and two parking spaces per unit with two or more bedrooms. Based on these rates, the project would need to provide a total of 228 parking spaces and would fall short of this by 30 spaces.

The project would qualify for State density bonus provisions as outlined in Government Code Section 65915, which requires one parking space for one-bedroom units and one and one-half parking spaces for two- and threebedroom units. Based on the unit mix for this project, 185 parking spaces are required, which equals the proposed supply. The proposed supply of 185 parking spaces is compliant with applicable State and local density bonus provisions.

The proposed parking supply's consistency with State density bonus provisions is shown in Table 10.
Table 10 - Parking Supply Consistency with State Density Bonus Provisions

| Land Use | Units | Rate | Parking Spaces |
| :--- | :---: | :---: | :---: |
| Multifamily Affordable Housing | 142 du |  |  |
| 1 bedroom | 56 du | $1.0 \mathrm{space} / \mathrm{du}$ | 56 |
| $2+$ bedrooms | 86 du | $1.5 \mathrm{spaces} / \mathrm{du}$ | 129 |
| State Required Parking Total |  |  | 185 |
| Proposed Parking Supply |  |  | $\mathbf{1 8 5}$ |

Notes: du=dwelling unit

It should be noted that the site is located within one-quarter mile of transit stops for Santa Rosa CityBus and would be connected to surrounding pedestrian and bicycle facilities, supporting travel by non-auto modes and reducing reliance on vehicle ownership, which thereby helps to reduce demand for parking.

Finding - The proposed project would satisfy applicable parking requirements established in State Density Bonus provisions.

## Bicycle Parking

The required bicycle parking supply was calculated to ensure adequacy under City requirements. Santa Rosa City Code Section 20-36.040 requires multifamily dwellings to provide bicycle parking at the rate of one space per four units if the units do not have a private garage or private storage space. The proposed project provides 41 longterm and 18 short-term bike spaces and would meet bike parking requirements.

Finding - The project's proposed bicycle parking would be adequate.

## Conclusions and Recommendations

## Conclusions

- The proposed project is expected to generate an average of 772 trips per day, including 51 a.m. peak hour trips and 62 trips during the p.m. peak hour.
- The study intersections are expected to continue operating acceptably at the same levels of service upon the addition of project-generated traffic. Although the southbound approach to Hearn Avenue/ Burbank Avenue is expected to operate at LOS F, the project's effect would be considered acceptable as the intersection would be expected to continue operating acceptably overall and the peak hour signalization warrant would be unmet.
- Under Baseline plus Project conditions the study intersections are expected to continue operating acceptably overall. Although the southbound approach at Hearn Avenue/Burbank Avenue is expected to operate at LOS $F$, the project's effect would be considered acceptable as the intersection would be expected to continue operating acceptably overall, the peak hour signal warrant would be met both without and with the project, and the project would be expected to increase overall delays by less than five seconds.
- The project would have a less-than-significant impact on vehicle miles traveled.
- Pedestrian facilities serving the project site would be adequate upon the completion of the proposed frontage improvements.
- Bicycle facilities serving the project site are adequate.
- Transit facilities serving the project site are adequate.
- Based on field observations and review of the project site plan, the project's proposed driveways are anticipated to operate acceptably, with adequate sight distances existing along Old Stony Point Road and Hearn Avenue.
- Emergency access is expected to function acceptably.
- Onsite circulation is anticipated to function acceptably.
- The Peak Hour Volume warrant would be met at the intersection of Hearn Avenue/Burbank Avenue under Baseline and Baseline plus Project volumes. The need for signalization was identified in the Roseland Area/Sebastopol Road Specific Plan, and the project has been added to the City's Capital Improvement Program.
- The proposed project would satisfy applicable parking requirements established in State Density Bonus provisions.
- The project's proposed bicycle parking would be adequate.


## Recommendations

- To maintain a clear line of sight from the project driveways, it is recommended that any landscaping be lowprofile, and that trees be set back outside the vision triangle.
- As directed by the City, the applicant should contribute a proportional share of funds for the signalization of the intersection of Hearn Avenue/Burbank Avenue. The project would be responsible for 9.3 percent of the cost, or \$29,760.


## Study Participants and References

## Study Participants

Principal in Charge<br>Assistant Engineer<br>Graphics<br>Editing/Formatting<br>Quality Control<br>Zack Matley, AICP<br>Kimberly Tellez<br>Cameron Wong<br>Cameron Wong<br>Dalene J. Whitlock, PE, PTOE

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SRO411


## Appendix A

## Collision Rate Calculations



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| Intersection Collision Rate Worksheet |  |  |  |
| :---: | :---: | :---: | :---: |
| Stony Oaks TIS |  |  |  |
| Intersection \# 3: Hearn Ave \& Old Stony Point Rd |  |  |  |
| Date of Count: Saturday, January 0,1900 |  |  |  |
|  |  |  |  |
| $\begin{aligned} \text { Number of Collisions: } & 2 \\ \text { Number of Injuries: } & 1\end{aligned}$ |  |  |  |
| Number of Fatalities: 0 Average Daily Traffic (ADT): 9000 |  |  |  |
|  |  |  |  |
| Start Date: November 1, 2014 |  |  |  |
| ```End Date: October 31, 2019``` |  |  |  |
|  |  |  |  |
| Intersection Type: Tee <br> Control Type: Stop \& Yield Controls <br> Area: Suburban |  |  |  |
|  |  |  |  |
|  |  |  |  |
| Collision Rate $=$ | Number of Collisions $\times 1$ Million |  |  |
|  | ADT $\times$ Days per Year $\times$ Number of Years |  |  |
| Collision Rate $=$ | 2 | $\mathrm{x} \quad 1,000,000$ |  |
|  | 9,000 x | 365 | $\times \quad 5$ |
| Study Intersection Statewide Average* | Collision Rate | Fatality Rate | Injury Rate |
|  | $0.12 \mathrm{c} / \mathrm{mve}$ | 0.0\% | 50.0\% |
|  | $0.14 \mathrm{c} / \mathrm{mve}$ | 1.2\% | 38.2\% |
| Notes |  |  |  |
| ADT = average daily total vehicles entering intersection $\mathrm{c} / \mathrm{mve}=$ collisions per million vehicles entering intersection <br> * 2016 Collision Data on California State Highways, Caltrans |  |  |  |
|  |  |  |  |
| Intersection \# 4: Hearn Ave \& Burbank Ave |  |  |  |
| Date of Count: Saturday, January 0, 1900 |  |  |  |
| Number of Collisions: 6 |  |  |  |
| Number of Collisions: 6 |  |  |  |
| Number of Fatalities: 0 <br> Average Daily Traffic (ADT): 13400 |  |  |  |
|  |  |  |  |
| Start Date: | 13400November 1, 2014 |  |  |
| End Date: October 31, 2019 |  |  |  |
| Number of Years: 5 |  |  |  |
| Intersection Type: Four-Legged <br> Control Type: Stop \& Yield Controls <br> Area: Suburban |  |  |  |
|  |  |  |  |
|  |  |  |  |
| Collision Rate $=$ Number of Collisions $\times 1$ Million |  |  |  |
| Collision Rate $=$ | ADT $\times$ Days per Year $\times$ Number of Years |  |  |
| Collision Rate $=$ | 6 | $x \quad 1,0$ | 1,000,000 |
|  | 13,400 x | 365 | $\times \quad 5$ |
| Study Intersection Statewide Average* | Collision Rate | Fatality Rate | Injury Rate |
|  | $0.25 \mathrm{c} / \mathrm{mve}$ | 0.0\% | 83.3\% |
|  | $0.23 \mathrm{c} / \mathrm{mve}$ | 1.9\% | 39.0\% |
| Notes <br> ADT = average daily total vehicles entering intersection $\mathrm{c} / \mathrm{mve}=$ collisions per million vehicles entering intersection * 2016 Collision Data on California State Highways, Caltrans |  |  |  |


| Intersection Collision Rate Worksheet |  |  |  |
| :---: | :---: | :---: | :---: |
| Stony Oaks TIS |  |  |  |
| Intersection \# 5: | Hearn Ave \& Dutton Meadow |  |  |
| Date of Count: Saturday, January 0, 1900 |  |  |  |
| Number of Collisions: 9 |  |  |  |
| Number of Injuries: 6 |  |  |  |
| Number of Fatalities: 0 |  |  |  |
| Start Date: | November 1, 2014October 31, 2019 |  |  |
| End Date: |  |  |  |
| Number of Years: |  |  |  |
| Intersection Type: Tee Control Type: Signals Area: Suburban |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Collision Rate $=$ | Number of Collisions $\times 1$ Million |  | ADT x Days per Year x Number of Years |
| Collision Rate $=$ | 9 | $\mathrm{x} \quad 1,000,000$ |  |
|  | 15,100 x | 365 | $\times \quad 5$ |
|  | Collision Rate | Fatality Rate | Injury Rate |
| Study Intersection Statewide Average* | $0.33 \mathrm{c} / \mathrm{mve}$ | 0.0\% | 66.7\% |
|  | $0.28 \mathrm{c} / \mathrm{mve}$ | 0.4\% | 37.2\% |
| Notes |  |  |  |
| ADT $=$ average daily total vehicles entering intersection |  |  |  |
| $\mathrm{c} / \mathrm{mve}=$ collisions per million vehicles entering intersection <br> * 2016 Collision Data on California State Highways, Caltrans |  |  |  |



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## Appendix B

Intersection Level of Service Calculations


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| HCM 6th Signalized Intersection Summary <br> 1：Stony Point Rd \＆Northpoint Pkwy |  |  |  |  |  |  |  |  |  |  | 02／03／2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\Rightarrow$ | $\rightarrow$ | 7 | $t$ | $\leftarrow$ |  | 4 | $\dagger$ | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ |  | F |  |  |  | \％ | 个的 |  | \％ | 个 ${ }_{\text {a }}$ |  |
| Traffic Volume（veh／h） | 58 | 0 | 189 | 0 | 0 | 0 | 392 | 807 | 0 | 0 | 818 | 116 |
| Future Volume（veh／h） | 58 | 0 | 189 | 0 | 0 | 0 | 392 | 807 | 0 | 0 | 818 | 116 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 0 | 1870 |  |  |  | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 58 | 0 | 189 |  |  |  | 392 | 807 | 0 | 0 | 818 | 116 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 0 | 2 |  |  |  | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 228 | 0 | 341 |  |  |  | 563 | 2830 | 0 | 67 | 2128 | 302 |
| Arrive On Green | 0.13 | 0.00 | 0.13 |  |  |  | 0.12 | 1.00 | 0.00 | 0.00 | 0.68 | 0.68 |
| Sat Flow，veh／h | 1781 | 0 | 1585 |  |  |  | 1781 | 3647 | 0 | 675 | 3124 | 443 |
| Grp Volume（v），veh／h | 58 | 0 | 189 |  |  |  | 392 | 807 | 0 | 0 | 465 | 469 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1585 |  |  |  | 1781 | 1777 | 0 | 675 | 1777 | 1791 |
| Q Serve（g＿s），s | 3.2 | 0.0 | 11.5 |  |  |  | 6.9 | 0.0 | 0.0 | 0.0 | 12.2 | 12.2 |
| Cycle Q Clear（ $\mathrm{c}_{\text {＿}}$ ），s | 3.2 | 0.0 | 11.5 |  |  |  | 6.9 | 0.0 | 0.0 | 0.0 | 12.2 | 12.2 |
| Prop In Lane | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.00 | 1.00 |  | 0.25 |
| Lane Grp Cap（c），veh／h | 228 | 0 | 341 |  |  |  | 563 | 2830 | 0 | 67 | 1210 | 1219 |
| VIC Ratio（X） | 0.25 | 0.00 | 0.55 |  |  |  | 0.70 | 0.29 | 0.00 | 0.00 | 0.38 | 0.38 |
| Avail Cap（c＿a），veh／h | 463 | 0 | 551 |  |  |  | 885 | 2830 | 0 | 67 | 1210 | 1219 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  |  |  | 1.33 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 0.00 | 1.00 |  |  |  | 0.79 | 0.79 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 42.5 | 0.0 | 37.7 |  |  |  | 5.6 | 0.0 | 0.0 | 0.0 | 7.4 | 7.4 |
| Incr Delay（d2），s／veh | 0.2 | 0.0 | 0.5 |  |  |  | 0.5 | 0.2 | 0.0 | 0.0 | 0.9 | 0.9 |
| Initial Q Delay（d3），S／veh | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.4 | 0.0 | 10.2 |  |  |  | 1.5 | 0.1 | 0.0 | 0.0 | 4.2 | 4.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 42.7 | 0.0 | 38.3 |  |  |  | 6.0 | 0.2 | 0.0 | 0.0 | 8.4 | 8.4 |
| LnGrp LOS | D | A | D |  |  |  | A | A | A | A | A | A |
| Approach Vol，veh／h |  | 247 |  |  |  |  |  | 1199 |  |  | 934 |  |
| Approach Delay，s／veh |  | 39.3 |  |  |  |  |  | 2.1 |  |  | 8.4 |  |
| Approach LOS |  | D |  |  |  |  |  | A |  |  | A |  |
| Timer－Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{C})$ ，$s$ |  | 89.9 |  | 18.1 | 12.5 | 77.4 |  |  |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ），$s$ |  | 3.9 |  | 4.3 | 3.0 | 3.9 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | 71.7 |  | 28.1 | 29.0 | 39.7 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  | 13.5 | 8.9 | 14.2 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 6.3 |  | 0.3 | 0.5 | 6.1 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 8.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |


| AM Existing | Synchro 11 Report |
| :--- | ---: |
| Stony Oaks TIS | Page 1 |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\stackrel{1}{5}$ |  | \％ | $\uparrow$ | F | \％ | $\uparrow$ | F | 7 | $\uparrow$ ¢ |  |
| Traffic Volume（veh／h） | 117 | 61 | 47 | 90 | 18 | 309 | 9 | 555 | 69 | 262 | 705 | 16 |
| Future Volume（veh／h） | 117 | 61 | 47 | 90 | 18 | 309 | 9 | 555 | 69 | 262 | 705 | 16 |

$\begin{array}{lllllllllllll}\text { Traffic Volume（veh／h）} & 117 & 61 & 47 & 90 & 18 & 309 & 9 & 555 & 69 & 262 & 705 & 1 \\ \text { Future Volume（veh／h）} & 117 & 61 & 47 & 90 & 18 & 309 & 9 & 555 & 69 & 262 & 705 & 16\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Initial Q（Qb），veh } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \text { Ped－Bike Adj（A＿pbT）} & 1.00 & & 1.00 & 1.00 & & 1.00 & 1.00 & & 1.00 & 1.00 & & 1.00\end{array}$
$\begin{array}{llllllllllllll}\text { Parking Bus，Adj } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$
$\begin{array}{lllllllllllllll}\text { Work Zone On Approach } & \text { No } & & & \text { No } & & & \text { No } & & & \text { No } \\ \text { Adj Sat Flow，veh／h／n } & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1945 & 1945 & 1870 & 1870 & 1870\end{array}$
$\begin{array}{lllllllllllll}\text { Adj Flow Rate，veh／h } & 117 & 61 & 47 & 90 & 18 & 309 & 9 & 555 & 69 & 262 & 705 & 16\end{array}$
$\begin{array}{lllllllllllll}\text { Peak Hour Factor } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$
$\begin{array}{llrrrrrrrrrr}\text { Percent Heavy Veh，} \% & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2\end{array}$

Cap，veh／h $\quad 132150121 \quad 114 \quad 284$ $\begin{array}{lllllllllllll}\text { Arrive On Green } & 0.07 & 0.16 & 0.16 & 0.06 & 0.15 & 0.15 & 0.18 & 0.47 & 0.47 & 0.05 & 0.14 & 0.1\end{array}$ | Sat |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Grp Volume（v），veh／h | 117 | 0 | 108 | 90 | 18 | 309 | 9 | 555 | 69 | 262 | 353 | 368 | Grp Sat Flow（s），veh／h／lin1781 $\begin{array}{lllllllllllll} & 0 & 1734 & 1781 & 1870 & 1585 & 1781 & 1945 & 1648 & 1781 & 1777 & 1856\end{array}$ $\begin{array}{lllllllllllllll}\text { Q Serve（g＿s），s } & 7.0 & 0.0 & 6.0 & 5.4 & 0.9 & 13.3 & 0.4 & 23.1 & 2.5 & 15.8 & 19.7 & 19.7\end{array}$ $\begin{array}{lllllllllllll}\text { Cycle Q Clear（g＿c），s } & 7.0 & 0.0 & 6.0 & 5.4 & 0.9 & 13.3 & 0.4 & 23.1 & 2.5 & 15.8 & 19.7 & 19.7\end{array}$ $\begin{array}{llllllllll}\text { Prop In Lane } & 1.00 & 0.44 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 0.04\end{array}$ $\begin{array}{lllllllllllll}\text { Lane Grp Cap（c），veh／h } & 132 & 0 & 279 & 114 & 284 & 501 & 329 & 905 & 767 & 293 & 763 & 797\end{array}$ $\begin{array}{lllllllllllll}\text { V／C Ratio（X）} & 0.89 & 0.00 & 0.39 & 0.79 & 0.06 & 0.62 & 0.03 & 0.61 & 0.09 & 0.89 & 0.46 & 0.4\end{array}$ $\begin{array}{lllllllllllll}\text { Avail Cap（c＿a），veh／h } & 132 & 0 & 514 & 148 & 571 & 745 & 329 & 905 & 767 & 297 & 763 & 79\end{array}$ Werm Fiterll $\quad 1.001 .001 .001001 .00$ Uniform Delay（d）s／veh 49．6 $\begin{array}{lllllllllllll}0.0 & 40.6 & 49.8 & 39.2 & 18.2 & 36.1 & 21.6 & 16.1 & 50.1 & 34.9 & 34.9\end{array}$

$$
\begin{array}{lrrrrrrrrr}
\text { Uniform Delay (d), s/veh 49.6 } & 0.0 & 40.6 & 49.8 & 39.2 & 18.2 & 36.1 & 21.6 & 16.1 & 50.1 \\
\hline & 34.9 & 34.0 \\
\text { Incr Delay (d2), s/veh } & 46.1 & 0.0 & 0.9 & 18.9 & 0.1 & 1.2 & 0.0 & 3.1 & 0.2 \\
\hline 24.5 & 1.8 & 1.8
\end{array}
$$

$$
\begin{array}{llllllllllll}
\text { Incr Delay (d2), s/veh } & 46.1 & 0.0 & 0.9 & 18.9 & 0.1 & 1.2 & 0.0 & 3.1 & 0.2 & 24.5 & 1.8 \\
\hline & 1.8 \\
\text { Initial Q Delayy (d3),s/veh } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0
\end{array} 0.0
$$

$$
\begin{array}{llllllllllll}
\begin{array}{l}
\text { \%ile BackOf(150\%),veh/Ir4.8.8 } \\
\text { Unsia Moven }
\end{array} 0.0 & 2.6 & 3.0 & 0.4 & 4.9 & 0.2 & 10.6 & 1.0 & 9.5 & 9.7 & 10.1
\end{array}
$$

$$
\begin{aligned}
& \text { Unsig. Movement Delay, siveh } \\
& \text { Uns. }
\end{aligned}
$$



| nGrp LOS | F | A | D | E | D | B | D | C | B | E | D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


|  | F | A | D | E | D | B | D | C | B | E |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | D


| Approach Delay，s／veh | 69.6 | 30.9 | 24.0 | 46.8 |
| :--- | ---: | ---: | ---: | ---: |
| Approach LOS | E | C | C | D |


| Approach LOS |  | E |  |  | C |  |  | C |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |

$\begin{array}{llllllll}\text { Phs Duration }(G+Y+R c), 30.8 & 54.9 & 10.9 & 21.4 & 24.6 & 51.1 & 12.0 & 20.3\end{array}$
$\begin{array}{lllllllll}\text { Change Period（Y＋Rc），} \mathrm{S} 3.0 & 4.7 & 4.0 & \text {＊} 4 & 4.7 & \text {＊} 4.7 & 4.0 & 3.9\end{array}$
$\begin{array}{llllllll}\text { Max Green Setting（Gmaxp．} & 33.4 & 9.0 & * 32 & 5.0 & * 46 & 8.0 & 33.0\end{array}$


| Intersection Summary |  |
| :--- | ---: |
| HCM 6th Ctrl Delay | 39.7 |
| HCM 6th LOS | $D$ |

## HCM 6th LOS

39.7
${ }^{*}$ NCM HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

## AM Existing

Stony Oaks TIS


| AM Existing | Synchro 11 Report |
| :--- | ---: |
| Stony Oaks TIS | Page 3 |



[^1]| HCM 6th Signalized Intersection Summary <br> 5: Hearn Ave \& Dutton Meadow |  |  |  |  |  |  |  |  |  |  | 02/03/2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{ }$ | $\rightarrow$ | 7 | $\checkmark$ | $\longleftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\downarrow$ | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{}$ |  | \% | $\uparrow$ |  |  | $\uparrow$ | F |  |  |  |
| Traffic Volume (veh/h) | 0 | 509 | 64 | 367 | 433 | 0 | 102 | 0 | 406 | 0 | 0 | 0 |
| Future Volume (veh/h) | 0 | 509 | 64 | 367 | 433 | 0 | 102 | 0 | 406 | 0 | 0 | 0 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1870 | 1870 | 1870 | 1870 | 0 | 1870 | 1870 | 1870 |  |  |  |
| Adj Flow Rate, veh/h | 0 | 509 | 64 | 367 | 433 | 0 | 102 | 0 | 406 |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Percent Heavy Veh, \% | 0 | 2 | 2 | 2 | 2 | 0 | 2 | 2 | 2 |  |  |  |
| Cap, veh/h | 0 | 612 | 77 | 427 | 1302 | 0 | 279 | 0 | 628 |  |  |  |
| Arrive On Green | 0.00 | 0.38 | 0.38 | 0.24 | 0.70 | 0.00 | 0.16 | 0.00 | 0.16 |  |  |  |
| Sat Flow, veh/h | 0 | 1629 | 205 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Grp Volume(v), veh/h | 0 | 0 | 573 | 367 | 433 | 0 | 102 | 0 | 406 |  |  |  |
| Grp Sat Flow(s),veh/h/n | 0 | 0 | 1833 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Q Serve(g_s), s | 0.0 | 0.0 | 12.7 | 8.8 | 4.1 | 0.0 | 2.3 | 0.0 | 0.0 |  |  |  |
| Cycle Q Clear (__c), s | 0.0 | 0.0 | 12.7 | 8.8 | 4.1 | 0.0 | 2.3 | 0.0 | 0.0 |  |  |  |
| Prop In Lane | 0.00 |  | 0.11 | 1.00 |  | 0.00 | 1.00 |  | 1.00 |  |  |  |
| Lane $\operatorname{Grp} \operatorname{Cap}(\mathrm{c})$, veh/h | 0 | 0 | 688 | 427 | 1302 | 0 | 279 | 0 | 628 |  |  |  |
| V/C Ratio(X) | 0.00 | 0.00 | 0.83 | 0.86 | 0.33 | 0.00 | 0.37 | 0.00 | 0.65 |  |  |  |
| Avail Cap(c_a), veh/h | 0 | 0 | 878 | 439 | 1482 | 0 | 718 | 0 | 1019 |  |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter(l) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |  |  |  |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 12.7 | 16.3 | 2.7 | 0.0 | 16.9 | 0.0 | 10.9 |  |  |  |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 5.5 | 14.6 | 0.1 | 0.0 | 0.8 | 0.0 | 1.1 |  |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \%ile BackOfQ(50\%),veh/n | 0.0 | 0.0 | 5.1 | 4.8 | 0.5 | 0.0 | 0.9 | 0.0 | 2.6 |  |  |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 0.0 | 0.0 | 18.2 | 30.9 | 2.8 | 0.0 | 17.7 | 0.0 | 12.1 |  |  |  |
| LnGrp LOS | A | A | B | C | A | A | B | A | B |  |  |  |
| Approach Vol, veh/h |  | 573 |  |  | 800 |  |  | 508 |  |  |  |  |
| Approach Delay, s/veh |  | 18.2 |  |  | 15.7 |  |  | 13.2 |  |  |  |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  |  |  |
| Timer - Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 14.3 | 20.4 |  |  |  | 34.7 |  | 10.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.6 | *3.6 |  |  |  | 3.6 |  | 3.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 11.0 | *21 |  |  |  | 35.4 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 10.8 | 14.7 |  |  |  | 6.1 |  | 4.3 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 2.1 |  |  |  | 2.9 |  | 1.7 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 15.8 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

HCM 6 th computational engine requires equal clearance times for the phases crossing the barrier.
AM Existing
Stony Oaks TIS

| HCM 6th Signalized I 1：Stony Point Rd \＆N | nters Northp | ction <br> oint P | Summ wwy |  |  |  |  |  |  |  |  | 02／03／2021 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ | $\rightarrow$ | $\geqslant$ | $\downarrow$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | 7 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ |  | F |  |  |  | 7 | 个t |  | \％ | 个t |  |
| Traffic Volume（veh／h） | 130 | 0 | 422 | 0 | 0 | 0 | 169 | 785 | 0 | 0 | 932 | 43 |
| Future Volume（veh／h） | 130 | 0 | 422 | 0 | 0 | 0 | 169 | 785 | 0 | 0 | 932 | 43 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／n | 1870 | 0 | 1870 |  |  |  | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 130 | 0 | 422 |  |  |  | 169 | 785 | 0 | 0 | 932 | 43 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 0 | 2 |  |  |  | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 171 | 0 | 736 |  |  |  | 837 | 2966 | 0 | 61 | 1498 | 69 |
| Arrive On Green | 0.10 | 0.00 | 0.10 |  |  |  | 0.74 | 1.00 | 0.00 | 0.00 | 0.43 | 0.43 |
| Sat Flow，veh／h | 1781 | 0 | 1585 |  |  |  | 1781 | 3647 | 0 | 689 | 3459 | 160 |
| Grp Volume（v），veh／h | 130 | 0 | 422 |  |  |  | 169 | 785 | 0 | 0 | 479 | 496 |
| Grp Sat Flow（s），veh／h／n | 1781 | 0 | 1585 |  |  |  | 1781 | 1777 | 0 | 689 | 1777 | 1842 |
| Q Serve（g＿s），s | 8.4 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 24.7 | 24.7 |
| Cycle Q Clear（g＿c），s | 8.4 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 24.7 | 24.7 |
| Prop In Lane | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.00 | 1.00 |  | 0.09 |
| Lane Grp Cap（c），veh／h | 171 | 0 | 736 |  |  |  | 837 | 2966 | 0 | 61 | 769 | 798 |
| V／C Ratio（X） | 0.76 | 0.00 | 0.57 |  |  |  | 0.20 | 0.26 | 0.00 | 0.00 | 0.62 | 0.62 |
| Avail Cap（c＿a），veh／h | 433 | 0 | 970 |  |  |  | 837 | 2966 | 0 | 61 | 769 | 798 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  |  |  | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 |  |  |  | 0.79 | 0.79 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 52.0 | 0.0 | 23.1 |  |  |  | 5.0 | 0.0 | 0.0 | 0.0 | 26.0 | 26.0 |
| Incr Delay（d2），s／veh | 2.6 | 0.0 | 0.3 |  |  |  | 0.0 | 0.2 | 0.0 | 0.0 | 3.8 | 3.6 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 3.8 | 0.0 | 13.9 |  |  |  | 0.9 | 0.1 | 0.0 | 0.0 | 10.8 | 11.2 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 54.7 | 0.0 | 23.3 |  |  |  | 5.1 | 0.2 | 0.0 | 0.0 | 29.7 | 29.6 |
| LnGrp LOS | D | A | C |  |  |  | A | A | A | A | C |  |
| Approach Vol，veh／h |  | 552 |  |  |  |  |  | 954 |  |  | 975 |  |
| Approach Delay，s／veh |  | 30.7 |  |  |  |  |  | 1.0 |  |  | 29.7 |  |
| Approach LOS |  | C |  |  |  |  |  | A |  |  | C |  |
| Timer－Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{RC}$ ）， S |  | 102.4 |  | 15.6 | 47.4 | 55.0 |  |  |  |  |  |  |
| Change Period（ $Y+R \mathrm{C}$ ），$s$ |  | 3.9 |  | 4.3 | 3.9 | ＊ 3.9 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | 81.1 |  | 28.7 | 27.0 | ＊51 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c ${ }^{\text {c }}$ ），s |  | 2.0 |  | 10.4 | 2.0 | 26.7 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 6.1 |  | 0.9 | 0.2 | 6.3 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 18.9 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\dagger$ |  | \％ | $\uparrow$ | \％ | $\dagger$ | $\uparrow$ | 7 | \％ | 个 4 |  |
| Traffic Volume（veh／h） | 42 | 22 | 23 | 117 | 34 | 286 | 40 | 672 | 116 | 268 | 758 | 29 |

$\begin{array}{lllllllllllll}\text { Traffic Volume（veh／h）} & 42 & 22 & 23 & 117 & 34 & 286 & 40 & 672 & 116 & 268 & 758 & 29 \\ \text { Future Volume（veh／h）} & 42 & 22 & 23 & 117 & 34 & 286 & 40 & 672 & 116 & 268 & 758 & 29\end{array}$ $\begin{array}{lrrrrrrrrrrrr}\text { Initial Q（Qb），veh } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$ $\begin{array}{lllllllllllll}\text { Parking Bus，Adj } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$
$\begin{array}{lllllllll}\text { Work Zone On Approach } & \text { No } & & \text { No } & \text { No } & & \text { No }\end{array}$
$\begin{array}{lllllllllllllll}\text { Adj Sat Flow，veh／h／ln } 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1945 & 1945 & 1870 & 1870 & 1870\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Adj Flow Rate，veh／h } & 42 & 22 & 23 & 117 & 34 & 286 & 40 & 672 & 116 & 268 & 758 & 29 \\ \text { Peak Hour Factor } & 100 & 100 & 100 & 100 & 100 & 100 & 100 & 100 & 100 & 100 & 100 & 100\end{array}$
$\begin{array}{lllllllllllll}\text { Peak Hour Factor } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Percent Heavy Ven，} & 2 & 2 & 2 & 29 & 136 & 167 & 720 & 55 & 715 & 606 & 650 & 2500 \\ \text { Cap，veh／h } & 54 & 37 & 39 & 136 & 96\end{array}$

$\begin{array}{lrrrrrrrrrrrr}\text { Cap，veh／h } & 54 & 37 & 39 & 136 & 167 & 720 & 55 & 715 & 606 & 650 & 2500 & 96 \\ \text { Arrive On Green } & 0.03 & 0.04 & 0.04 & 0.08 & 0.09 & 0.09 & 0.03 & 0.37 & 0.37 & 0.73 & 1.00 & 1.00\end{array}$ | Arrive On Green | 0.03 | 0.04 | 0.04 | 0.08 | 0.09 | 0.09 | 0.03 | 0.37 | 0.37 | 0.73 | 1.00 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Srit Flow，veh／h | 1781 | 837 | 875 | 1781 | 1870 | 1585 | 1781 | 1945 | 1648 | 1781 | 3490 |
| Sat |  | 133 |  |  |  |  |  |  |  |  |  | $\begin{array}{llllllllllllll}\text { Grp Volume（v），veh／h } & 42 & 0 & 45 & 117 & 34 & 286 & 40 & 672 & 116 & 268 & 386 & 401\end{array}$

 $\begin{array}{llllllllllllll}\text { Q Serve（g＿s），s } & 2.8 & 0.0 & 3.0 & 7.7 & 2.0 & 1.7 & 2.6 & 39.4 & 5.6 & 6.9 & 0.0 & 0.0\end{array}$ $\begin{array}{lllllllllllll}\text { Cycle Q Clear（g＿c），s } & 2.8 & 0.0 & 3.0 & 7.7 & 2.0 & 1.7 & 2.6 & 39.4 & 5.6 & 6.9 & 0.0\end{array}$ $\begin{array}{lllllllll}\text { Prop In Lane } & 1.00 & 0.51 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 0.07\end{array}$ $\begin{array}{lllllllllllll}\text { Lane Grp Cap（c），veh／h } & 54 & 0 & 76 & 136 & 167 & 720 & 55 & 715 & 606 & 650 & 1273 & 132\end{array}$ $\begin{array}{lllllllllllll}\text { V／C Ratio（X）} & 0.78 & 0.00 & 0.59 & 0.86 & 0.20 & 0.40 & 0.73 & 0.94 & 0.19 & 0.41 & 0.30 & 0.30\end{array}$ $\begin{array}{lllllllllllll}\text { Avail Cap（c＿a），veh／h } & 106 & 0 & 450 & 136 & 523 & 1022 & 106 & 715 & 606 & 650 & 1273 & 132\end{array}$ Ulustream Filter（l） $1.100 \quad 0.00$ 1．00 1.0100 $\begin{array}{lllllllllllll}\text { Uniform Delay（d）．s／veh 56．8 } & 0.0 & 55.4 & 53.9 & 49.8 & 12.3 & 56.7 & 36.0 & 25.4 & 11.0 & 0.0 & 0.0\end{array}$
$\begin{array}{llllllllllllll}\text { Incr Delay（d2），s／veh } & 21.1 & 0.0 & 7.2 & 39.4 & 0.6 & 0.4 & 6.6 & 21.7 & 0.7 & 0.1 & 0.5 & 0.5\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Incr Delay（d2），slveh } & 21.1 & 0.0 & 7.2 & 39.4 & 0.6 & 0.4 & 6.6 & 21.7 & 0.7 & 0.1 & 0.5 & 0.5 \\ \text { Initial Q Delay（d3）s／veh } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0\end{array}$
\％ile BackOfQ（50\％），veh／Ir1．6 $0.0 \begin{array}{lllllllllll}1.5 & 4.9 & 1.0 & 3.7 & 1.3 & 22.2 & 2.3 & 2.1 & 0.2 & 0.2\end{array}$
Unsig．Movement Delay，s／veh

| LnGrp Delay（d），S／veh | 77.9 | 0.0 | 62.6 | 93.3 | 50.4 | 12.6 | 63.3 | 57.7 | 26.1 | 11.2 | 0.5 | 0.5 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |



|  | A |  | B | E | C | B |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Vol，veh／h | 87 | 437 | 828 | 1055 |  |  |
| Approach Delay，slveh | 70.0 | 37.2 | 53.6 | 3.2 |  |  |
| Approach LOS | E |  |  |  |  |  |


| Approach Delay，s／veh | 70.0 | 37.2 | 53.6 | 3.2 |
| :--- | :---: | :---: | :---: | :---: |
| Approach LOS | E | D | D | A |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c), 47.8$ | 48.1 | 13.0 | 9.1 | 6.7 | 89.2 | 76 | 14.6 |  |

$\begin{array}{llllllll}\text { Phs Duration }(G+Y+R c), 47.8 & 48.1 & 13.0 & 9.1 & 6.7 & 89.2 & 7.6 & 14.6\end{array}$
Change Period（ $Y+R \mathrm{Rc}$ ），s 4.7 ＊ 4.7 4．0 $3.0 \begin{array}{llllll} & 3.0 & 4.7 & 4.0 & \text {＊4 }\end{array}$
$\begin{array}{lrrrrrrr}\text { Max Green Setting（Gmax9，} 8 & * 43 & 9.0 & 31.0 & 7.0 & 55.4 & 7.0 & * 33 \\ \text { Max Q Clear Time }(\mathrm{g} \mathrm{c}+18, \mathrm{~s} & 41.4 & 9.7 & 5.0 & 4.6 & 2.0 & 4.8 & 4.0\end{array}$


## ntersection Summar

6th LOS
29.1
C
$\frac{\text { Notes }}{\text {＊HCM } 6 \text { th computational engine requires equal clearance times for the phases crossing the barrier．}}$


| PM Existing | Synchro 11 Report |
| :--- | ---: |
| Stony Oaks TIS | Page 3 |



[^2]| HCM 6th Signalized Intersection Summary <br> 5: Hearn Ave \& Dutton Meadow |  |  |  |  |  |  |  |  |  |  | 02/03/2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{ }$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\downarrow$ | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{}$ |  | \% | $\uparrow$ |  |  | $\uparrow$ | F |  |  |  |
| Traffic Volume (veh/h) | 0 | 409 | 57 | 218 | 594 | 0 | 112 | 0 | 273 | 0 | 0 | 0 |
| Future Volume (veh/h) | 0 | 409 | 57 | 218 | 594 | 0 | 112 | 0 | 273 | 0 | 0 | 0 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1870 | 1870 | 1870 | 1870 | 0 | 1870 | 1870 | 1870 |  |  |  |
| Adj Flow Rate, veh/h | 0 | 409 | 57 | 218 | 594 | 0 | 112 | 0 | 273 |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Percent Heavy Veh, \% | 0 | 2 | 2 | 2 | 2 | 0 | 2 | 2 | 2 |  |  |  |
| Cap, veh/h | 0 | 560 | 78 | 309 | 1165 | 0 | 342 | 0 | 579 |  |  |  |
| Arrive On Green | 0.00 | 0.35 | 0.35 | 0.17 | 0.62 | 0.00 | 0.19 | 0.00 | 0.19 |  |  |  |
| Sat Flow, veh/h | 0 | 1606 | 224 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Grp Volume(v), veh/h | 0 | 0 | 466 | 218 | 594 | 0 | 112 | 0 | 273 |  |  |  |
| Grp Sat Flow(s),veh/h/n | 0 | 0 | 1830 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Q Serve(g_s), s | 0.0 | 0.0 | 7.9 | 4.1 | 6.3 | 0.0 | 1.9 | 0.0 | 0.0 |  |  |  |
| Cycle Q Clear (__c), s | 0.0 | 0.0 | 7.9 | 4.1 | 6.3 | 0.0 | 1.9 | 0.0 | 0.0 |  |  |  |
| Prop In Lane | 0.00 |  | 0.12 | 1.00 |  | 0.00 | 1.00 |  | 1.00 |  |  |  |
| Lane $\operatorname{Grp} \operatorname{Cap}(\mathrm{c})$, veh/h | 0 | 0 | 638 | 309 | 1165 | 0 | 342 | 0 | 579 |  |  |  |
| V/C Ratio(X) | 0.00 | 0.00 | 0.73 | 0.70 | 0.51 | 0.00 | 0.33 | 0.00 | 0.47 |  |  |  |
| Avail Cap(c_a), veh/h | 0 | 0 | 1201 | 599 | 2014 | 0 | 899 | 0 | 1075 |  |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter(l) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |  |  |  |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 10.2 | 13.9 | 3.7 | 0.0 | 12.4 | 0.0 | 8.7 |  |  |  |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 1.6 | 1.1 | 0.3 | 0.0 | 0.6 | 0.0 | 0.6 |  |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \%ile BackOfQ(50\%),veh/n | 0.0 | 0.0 | 2.5 | 1.4 | 0.9 | 0.0 | 0.6 | 0.0 | 1.1 |  |  |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 0.0 | 0.0 | 11.8 | 15.0 | 4.1 | 0.0 | 13.0 | 0.0 | 9.3 |  |  |  |
| LnGrp LOS | A | A | B | B | A | A | B | A | A |  |  |  |
| Approach Vol, veh/h |  | 466 |  |  | 812 |  |  | 385 |  |  |  |  |
| Approach Delay, s/veh |  | 11.8 |  |  | 7.0 |  |  | 10.3 |  |  |  |  |
| Approach LOS |  | B |  |  | A |  |  | B |  |  |  |  |
| Timer - Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 9.8 | 16.0 |  |  |  | 25.8 |  | 9.8 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.6 | *3.6 |  |  |  | 3.6 |  | 3.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 12.0 | *23 |  |  |  | 38.4 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 6.1 | 9.9 |  |  |  | 8.3 |  | 3.9 |  |  |  |  |
| Green Ext Time (p_c), s | 0.2 | 2.5 |  |  |  | 4.4 |  | 1.3 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 9.1 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |


| HCM 6th Signalized <br>  | nters North | ction int P | Summ wy |  |  |  |  |  |  |  | 02/11/2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ | $\rightarrow$ |  | $t$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% |  | F |  |  |  | \% | 性 |  | \% | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (veh/h) | 58 | 0 | 195 | 0 | 0 | 0 | 397 | 898 | 0 | 0 | 856 | 116 |
| Future Volume (veh/h) | 58 | 0 | 195 | 0 | 0 | 0 | 397 | 898 | 0 | 0 | 856 | 116 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 0 | 1870 |  |  |  | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 58 | 0 | 195 |  |  |  | 397 | 898 | 0 | 0 | 856 | 116 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 2 | 0 | 2 |  |  |  | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 233 | 0 | 350 |  |  |  | 547 | 2818 | 0 | 67 | 2124 | 288 |
| Arrive On Green | 0.13 | 0.00 | 0.13 |  |  |  | 0.12 | 1.00 | 0.00 | 0.00 | 0.68 | 0.68 |
| Sat Flow, veh/h | 1781 | 0 | 1585 |  |  |  | 1781 | 3647 | 0 | 620 | 3144 | 426 |
| Grp Volume(v), veh/h | 58 | 0 | 195 |  |  |  | 397 | 898 | 0 | 0 | 484 | 488 |
| Grp Sat Flow(s), veh/h/n | 1781 | 0 | 1585 |  |  |  | 1781 | 1777 | 0 | 620 | 1777 | 1794 |
| Q Serve(g_s), s | 3.2 | 0.0 | 11.8 |  |  |  | 7.2 | 0.0 | 0.0 | 0.0 | 13.1 | 13.1 |
| Cycle Q Clear(g_c), s | 3.2 | 0.0 | 11.8 |  |  |  | 7.2 | 0.0 | 0.0 | 0.0 | 13.1 | 13.1 |
| Prop In Lane | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.00 | 1.00 |  | 0.24 |
| Lane Grp Cap(c), veh/h | 233 | 0 | 350 |  |  |  | 547 | 2818 | 0 | 67 | 1200 | 1212 |
| V/C Ratio(X) | 0.25 | 0.00 | 0.56 |  |  |  | 0.73 | 0.32 | 0.00 | 0.00 | 0.40 | 0.40 |
| Avail Cap(c_a), veh/h | 463 | 0 | 555 |  |  |  | 866 | 2818 | 0 | 67 | 1200 | 1212 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  |  |  | 1.33 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 |  |  |  | 0.72 | 0.72 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 42.2 | 0.0 | 37.4 |  |  |  | 6.2 | 0.0 | 0.0 | 0.0 | 7.8 | 7.8 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 0.5 |  |  |  | 0.5 | 0.2 | 0.0 | 0.0 | 1.0 | 1.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%oile BackOfQ(50\%),veh/ln | 1.4 | 0.0 | 10.5 |  |  |  | 1.6 | 0.1 | 0.0 | 0.0 | 4.6 | 4.6 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 42.4 | 0.0 | 37.9 |  |  |  | 6.7 | 0.2 | 0.0 | 0.0 | 8.8 | 8.8 |
| LnGrp LOS | D | A | D |  |  |  | A | A | A | A | A | A |
| Approach Vol, veh/h |  | 253 |  |  |  |  |  | 1295 |  |  | 972 |  |
| Approach Delay, s/veh |  | 38.9 |  |  |  |  |  | 2.2 |  |  | 8.8 |  |
| Approach LOS |  | D |  |  |  |  |  | A |  |  | A |  |
| Timer - Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{C})$, $s$ |  | 89.6 |  | 18.4 | 12.7 | 76.9 |  |  |  |  |  |  |
| Change Period ( $Y+R \mathrm{c}$ ), s |  | 3.9 |  | 4.3 | 3.0 | 3.9 |  |  |  |  |  |  |
| Max Green Setting (Gmax), s |  | 71.7 |  | 28.1 | 29.0 | 39.7 |  |  |  |  |  |  |
| Max Q Clear Time (g_c+11), s |  | 2.0 |  | 13.8 | 9.2 | 15.1 |  |  |  |  |  |  |
| Green Ext Time (p_c), s |  | 7.3 |  | 0.3 | 0.5 | 6.4 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 8.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |

AM Baseline
Stony Oaks TIS
Stony Oaks TIS

# EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL 


$\begin{array}{lllllllllllll}\text { Iraffic Volume (veh/h) } & 117 & 64 & 47 & 101 & 27 & 342 & 9 & 618 & 93 & 285 & 726 & 1 \\ \text { Future Volume (veh/h) } & 117 & 64 & 47 & 101 & 27 & 342 & 9 & 618 & 93 & 285 & 726 & 1\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Initial Q Q (Qb), veh } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \text { Ped-Bike Adj(A pbT) } & 1.00 & & 1.00 & 1.00 & & 1.00 & 1.00 & & 1.00 & 1.00 & & 1.00\end{array}$
$\begin{array}{lllllllllllll}\text { Parking Bus, Adj } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$
$\begin{array}{lllllllllllllll}\text { Work Zone On Approach } & \text { No } & & & \text { No } & & & \text { No } & & & \text { No } \\ \text { Adj Sat Flow, veh/h/n } & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1945 & 1945 & 1870 & 1870 & 1870\end{array}$
$\begin{array}{llllllllllllll}\text { Adj Flow Rate, veh/h } & 117 & 64 & 47 & 101 & 27 & 342 & 9 & 618 & 93 & 285 & 726 & 16\end{array}$

| Adj Flow Rate, veh/h | 117 | 64 | 47 | 101 | 27 | 34 | 9 | 618 | 93 | 285 | 726 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |

Percent Heavy Veh, \% $2 \begin{array}{lllllllllll} & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2\end{array}$
$\begin{array}{lllllllllllll}\text { Cap, veh/h } & 132 & 168 & 123 & 126 & 309 & 526 & 304 & 874 & 741 & 297 & 1527 & 34 \\ \text { Ariven } & 132 & 127 & & \end{array}$
$\begin{array}{lllllllllllll}\text { Arrive On Green } & 0.07 & 0.17 & 0.17 & 0.07 & 0.17 & 0.17 & 0.17 & 0.45 & 0.45 & 0.06 & 0.14 & 0.1 \\ \text { Sat Flow, veh/h } & 1781 & 1002 & 736 & 1781 & 1870 & 1585 & 1781 & 1945 & 1648 & 1781 & 3555 & 7\end{array}$
$\begin{array}{lllllllllllll}\text { Grp Volume(v), veh/h } & 117 & 0 & 111 & 101 & 27 & 342 & 9 & 618 & 93 & 285 & 363 & 379\end{array}$
Grp Sat Flow(s),veh/h/ln1781 $\begin{array}{llllllllllllll} & 0 & 1738 & 1781 & 1870 & 1585 & 1781 & 1945 & 1648 & 1781 & 1777 & 1856\end{array}$
$\begin{array}{lllllllllllll}\text { Q Serve(g_s), s } & 7.0 & 0.0 & 6.1 & 6.0 & 1.3 & 14.6 & 0.5 & 27.7 & 3.6 & 17.2 & 20.3 & 20.3\end{array}$
$\begin{array}{llllllllllllll}\text { Cycle Q Clear(g_c), s } & 7.0 & 0.0 & 6.1 & 6.0 & 1.3 & 14.6 & 0.5 & 27.7 & 3.6 & 17.2 & 20.3 & 20.3\end{array}$
$\begin{array}{llllllllll}\text { Prop In Lane } & 1.00 & 0.42 & 1.00 & & 1.00 & 1.00 & 1.00 & 1.00 & 0.04\end{array}$
Lane Grp Cap(c), veh/h $1320 \begin{array}{lllllllllll} & 029 & 126 & 309 & 526 & 304 & 874 & 741 & 297 & 763 & 798\end{array}$
$\begin{array}{lllllllllllll}\text { V/C Ratio(X) } & 0.89 & 0.00 & 0.38 & 0.80 & 0.09 & 0.65 & 0.03 & 0.71 & 0.13 & 0.96 & 0.48 & 0.48\end{array}$
$\begin{array}{lllllllllllll}\text { Avail Cap(c_a), veh/h } & 132 & 0 & 515 & 148 & 571 & 748 & 304 & 874 & 741 & 297 & 763 & 798\end{array}$

Uniform Delay (d) s/veh $49.610 .0 \begin{array}{lllllllllllll} & 40.0 & 49.4 & 38.2 & 17.6 & 37.3 & 24.0 & 17.4 & 50.7 & 35.1 & 35 .\end{array}$
$\begin{array}{lllllllllllll}\text { Incr Delay (d2), s/veh } & 46.1 & 0.0 & 0.8 & 22.6 & 0.1 & 1.4 & 0.0 & 4.8 & 0.3 & 38.6 & 1.9 & 1.8\end{array}$
$\begin{array}{llllllllllllll}\text { Incr Delay (d2), slveh } & 46.1 & 0.0 & 0.8 & 22.6 & 0.1 & 1.4 & 0.0 & 4.8 & 0.3 & 38.6 & 1.9 & 1.8 \\ \text { Initial Q Delay (d3),s/veh } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0\end{array}$
\%ile BackOfQ(50\%),veh/ra4.8 $00.0 \begin{array}{lllllllllll} & 2.7 & 3.5 & 0.6 & 5.4 & 0.2 & 13.1 & 1.4 & 11.4 & 10.0 & 10.4\end{array}$
Unsig. Movement Delay, slveh

LnGrp LOS $\quad$ F $\quad$ A $\quad$ D $\quad$ E $\quad$ D $\quad$ B $\quad$ D $\quad$ C

| Approach Vol, veh/h | 228 | 470 | 720 | 1027 |
| :--- | ---: | ---: | ---: | ---: |
| Approach Delay, s/veh | 68.9 | 31.5 | 27.5 | 51.5 |


| Approach Delay, s/veh | 68.9 | 31.5 | 27.5 | 51.5 |
| :--- | ---: | ---: | ---: | ---: |
| Approach LOS | E | C | C | D |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ 81.0 | 532 | 11.7 | 22.1 | 23.1 | 51.1 | 120 | 21.8 |  |

$\begin{array}{lllllllll} \\ \text { Duration }(G+Y+R C), 81.0 & 53.2 & 11.7 & 22.1 & 23.1 & 51.1 & 12.0 & 21.8\end{array}$
$\begin{array}{lllllllll}\text { Change Period (Y+Rc), } 3.0 & 4.7 & 4.0 & \text { * } 4 & 4.7 & \text { * } 4.7 & 4.0 & 3.9\end{array}$
$\begin{array}{llllllll}\text { Max Green Setting (Gmaxq. © } & 33.4 & 9.0 & * 32 & 5.0 & 46 & 8.0 & 33.0 \\ \text { Max Q Clear Time ( } \mathrm{g}+\mathrm{c}+\mathrm{HIT}, \mathrm{z} & 29.7 & 8.0 & 8.1 & 2.5 & 22.3 & 9.0 & 16.6\end{array}$
$\begin{array}{llllllll}\text { Max Q Clear Time (g_c+179,2s } & 29.7 & 8.0 & 8.1 & 2.5 & 22.3 & 9.0 & 16.6 \\ \text { Green Ext Time (p_c), s } & 0.0 & 1.5 & 0.0 & 0.6 & 0.0 & 4.4 & 0.0 \\ 1.2\end{array}$
Intersection Summary
HCM 6 th Ctrl Dela
$\frac{\text { Notes }}{*}$ HCM 6 th computational engine requires equal clearance times for the phases crossing the barrier

## AM Baseline

Stony Oaks TIS

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WB | BT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations | \% | $\uparrow$ |  |  |  | A |  | ¢ |  |  |  |  |  |  |
| Traffic Vol, veh/h | 7 | 427 | 0 | 0 |  | 48 | 2 | 0 | 0 | 0 | 9 | 0 | 15 |  |
| Future Vol, veh/h | 7 | 427 | 0 | 0 |  | 48 | 2 | 0 | 0 | 0 | 9 | 0 | 15 |  |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Free | Free | Free | Free | Fre | ree | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - |  | - | None | - | - | None | - | . | None |  |
| Storage Length | 65 | - | - | - |  | - | - | - | - | - | . | - | . |  |
| Veh in Median Storage, | \# | 0 | - |  |  | 0 |  | 10823 | 9328 |  |  | 1 |  |  |
| Grade, \% | - | 0 | - | - |  | 0 |  | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 |  | 00 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 |  | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mumt Flow | 7 | 427 | 0 | 0 |  | 48 | 2 | 0 | 0 | 0 | 9 | 0 | 15 |  |
| Major/Minor Ma | ajor1 |  | Major2 |  |  |  |  | Minor2 |  |  |  |  |  |  |
| Conflicting Flow All | 450 | 0 | - | - |  | - | 0 |  |  |  | 890 | 890 | 449 |  |
| Stage 1 | - | - | - | - |  | - | - |  |  |  | 449 | 449 | - |  |
| Stage 2 | - | - | - | - |  | - |  |  |  |  | 441 | 441 | - |  |
| Critical Hdwy | 4.12 | - | - | - |  | - | - |  |  |  | 6.42 | 6.52 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - |  | - | - |  |  |  | 5.42 | 5.52 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - |  | - | - |  |  |  | 5.42 | 5.52 | $\cdot$ |  |
| Follow-up Hdwy | 2.218 | - | - | - |  | - | - |  |  |  | 3.518 | 4.018 | 3.318 |  |
| Pot Cap-1 Maneuver | 1110 | - | 0 | 0 |  | - | - |  |  |  | 313 | 282 | 610 |  |
| Stage 1 | - | - | 0 | 0 |  | - | - |  |  |  | 643 | 572 | - |  |
| Stage 2 | - | - | 0 | 0 |  | - | - |  |  |  | 648 | 577 | - |  |
| Platoon blocked, \% |  | - |  |  |  | - | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1110 | - | - | - |  | - |  |  |  |  | 311 | 0 | 610 |  |
| Mov Cap-2 Maneuver | - | - | - | - |  | - |  |  |  |  | 436 | 0 | - |  |
| Stage 1 | - | - | - | - |  | - |  |  |  |  | 639 | 0 | - |  |
| Stage 2 | - | - | - | - |  | - |  |  |  |  | 648 | 0 | - |  |
| Approach | EB |  |  | WB |  |  |  |  |  |  | SB |  |  |  |
| HCM Control Delay, s | 0.1 |  |  | 0 |  |  |  |  |  |  | 12.1 |  |  |  |
| HCM LOS |  |  |  |  |  |  |  |  |  |  | B |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT |  | RR | SBLn1 |  |  |  |  |  |  |  |
| Capacity (veh/h) |  | 1110 | - | - |  | - | 531 |  |  |  |  |  |  |  |
| HCM Lane V/C Ratio |  | 0.006 | - | - |  | - | 0.045 |  |  |  |  |  |  |  |
| HCM Control Delay (s) |  | 8.3 | - | - |  | - | 12.1 |  |  |  |  |  |  |  |
| HCM Lane LOS |  | A | - | - |  | - | B |  |  |  |  |  |  |  |
| HCM 95th \%tile Q(veh) |  | 0 | - | - |  | - | 0.1 |  |  |  |  |  |  |  |



[^3]| HCM 6th Signalized <br> 5: Hearn Ave \& Dutto | nters | ction dow |  |  |  |  |  |  |  |  |  | 2021 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{ }$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\stackrel{ }{ }$ |  | \% | $\uparrow$ |  |  | $\uparrow$ | F |  |  |  |
| Traffic Volume (veh/h) | 0 | 556 | 79 | 388 | 461 | 0 | 134 | 0 | 468 | 0 | 0 | 0 |
| Future Volume (veh/h) | 0 | 556 | 79 | 388 | 461 | 0 | 134 | 0 | 468 | 0 | 0 | 0 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1870 | 1870 | 1870 | 1870 | 0 | 1870 | 1870 | 1870 |  |  |  |
| Adj Flow Rate, veh/h | 0 | 556 | 79 | 388 | 461 | 0 | 134 | 0 | 468 |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Percent Heavy Veh, \% | 0 | 2 | 2 | 2 | 2 | 0 | 2 | 2 | 2 |  |  |  |
| Cap, veh/h | 0 | 637 | 90 | 414 | 1320 | 0 | 276 | 0 | 614 |  |  |  |
| Arrive On Green | 0.00 | 0.40 | 0.40 | 0.23 | 0.71 | 0.00 | 0.16 | 0.00 | 0.16 |  |  |  |
| Sat Flow, veh/h | 0 | 1602 | 228 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Grp Volume(v), veh/h | 0 | 0 | 635 | 388 | 461 | 0 | 134 | 0 | 468 |  |  |  |
| Grp Sat Flow(s),veh/h/n | 0 | 0 | 1829 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Q Serve(g_s), s | 0.0 | 0.0 | 15.2 | 10.1 | 4.6 | 0.0 | 3.3 | 0.0 | 1.2 |  |  |  |
| Cycle Q Clear (__c), s | 0.0 | 0.0 | 15.2 | 10.1 | 4.6 | 0.0 | 3.3 | 0.0 | 1.2 |  |  |  |
| Prop In Lane | 0.00 |  | 0.12 | 1.00 |  | 0.00 | 1.00 |  | 1.00 |  |  |  |
| Lane $\operatorname{Grp} \operatorname{Cap}(\mathrm{c})$, veh/h | 0 | 0 | 727 | 414 | 1320 | 0 | 276 | 0 | 614 |  |  |  |
| V/C Ratio(X) | 0.00 | 0.00 | 0.87 | 0.94 | 0.35 | 0.00 | 0.49 | 0.00 | 0.76 |  |  |  |
| Avail Cap(c_a), veh/h | 0 | 0 | 826 | 414 | 1398 | 0 | 677 | 0 | 970 |  |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter(l) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |  |  |  |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 13.2 | 17.8 | 2.7 | 0.0 | 18.3 | 0.0 | 12.6 |  |  |  |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 9.3 | 28.7 | 0.2 | 0.0 | 1.3 | 0.0 | 2.0 |  |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \%ile BackOfQ(50\%),veh/n | 0.0 | 0.0 | 6.8 | 6.9 | 0.7 | 0.0 | 1.3 | 0.0 | 3.6 |  |  |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 0.0 | 0.0 | 22.5 | 46.6 | 2.9 | 0.0 | 19.6 | 0.0 | 14.6 |  |  |  |
| LnGrp LOS | A | A | C | D | A | A | B | A | B |  |  |  |
| Approach Vol, veh/h |  | 635 |  |  | 849 |  |  | 602 |  |  |  |  |
| Approach Delay, s/veh |  | 22.5 |  |  | 22.9 |  |  | 15.7 |  |  |  |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  |  |  |
| Timer - Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 14.6 | 22.4 |  |  |  | 37.0 |  | 10.3 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.6 | *3.6 |  |  |  | 3.6 |  | 3.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 11.0 | *21 |  |  |  | 35.4 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 12.1 | 17.2 |  |  |  | 6.6 |  | 5.3 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 1.6 |  |  |  | 3.1 |  | 2.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 20.7 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |


| HCM 6th Signalized I 1：Stony Point Rd \＆N | nters Northp | ction <br> oint P | Summ wwy |  |  |  |  |  |  |  | 02／11／2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ | $\rightarrow$ | $\geqslant$ | $\downarrow$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | 7 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ |  | F |  |  |  | \％ | 个t |  | \％ | 个t |  |
| Traffic Volume（veh／h） | 130 | 0 | 424 | 0 | 0 | 0 | 174 | 847 | 0 | 0 | 1028 | 43 |
| Future Volume（veh／h） | 130 | 0 | 424 | 0 | 0 | 0 | 174 | 847 | 0 | 0 | 1028 | 43 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／n | 1870 | 0 | 1870 |  |  |  | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 130 | 0 | 424 |  |  |  | 174 | 847 | 0 | 0 | 1028 | 43 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 0 | 2 |  |  |  | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 171 | 0 | 736 |  |  |  | 811 | 2966 | 0 | 61 | 1505 | 63 |
| Arrive On Green | 0.10 | 0.00 | 0.10 |  |  |  | 0.74 | 1.00 | 0.00 | 0.00 | 0.43 | 0.43 |
| Sat Flow，veh／h | 1781 | 0 | 1585 |  |  |  | 1781 | 3647 | 0 | 650 | 3476 | 145 |
| Grp Volume（v），veh／h | 130 | 0 | 424 |  |  |  | 174 | 847 | 0 | 0 | 526 | 545 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1585 |  |  |  | 1781 | 1777 | 0 | 650 | 1777 | 1844 |
| Q Serve（g＿s），s | 8.4 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 28.1 | 28.1 |
| Cycle Q Clear（g＿c），s | 8.4 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 28.1 | 28.1 |
| Prop In Lane | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.00 | 1.00 |  | 0.08 |
| Lane Grp Cap（c），veh／h | 171 | 0 | 736 |  |  |  | 811 | 2966 | 0 | 61 | 769 | 799 |
| VIC Ratio（X） | 0.76 | 0.00 | 0.58 |  |  |  | 0.21 | 0.29 | 0.00 | 0.00 | 0.68 | 0.68 |
| Avail Cap（c＿a），veh／h | 433 | 0 | 970 |  |  |  | 811 | 2966 | 0 | 61 | 769 | 799 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  |  |  | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 |  |  |  | 0.76 | 0.76 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 52.0 | 0.0 | 23.1 |  |  |  | 5.9 | 0.0 | 0.0 | 0.0 | 26.9 | 26.9 |
| Incr Delay（d2），s／veh | 2.6 | 0.0 | 0.3 |  |  |  | 0.0 | 0.2 | 0.0 | 0.0 | 4.9 | 4.7 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 3.8 | 0.0 | 13.9 |  |  |  | 1.0 | 0.1 | 0.0 | 0.0 | 12.4 | 12.8 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 54.7 | 0.0 | 23.4 |  |  |  | 5.9 | 0.2 | 0.0 | 0.0 | 31.8 | 31.6 |
| LnGrp LOS | D | A | C |  |  |  | A | A | A | A | C |  |
| Approach Vol，veh／h |  | 554 |  |  |  |  |  | 1021 |  |  | 1071 |  |
| Approach Delay，s／veh |  | 30.7 |  |  |  |  |  | 1.2 |  |  | 31.7 |  |
| Approach LOS |  | C |  |  |  |  |  | A |  |  | C |  |
| Timer－Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{RC}$ ）， S |  | 102.4 |  | 15.6 | 47.4 | 55.0 |  |  |  |  |  |  |
| Change Period（ $Y+R \mathrm{C}$ ），$s$ |  | 3.9 |  | 4.3 | 3.9 | ＊ 3.9 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | 81.1 |  | 28.7 | 27.0 | ＊51 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c ${ }^{\text {c }}$ ），s |  | 2.0 |  | 10.4 | 2.0 | 30.1 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 6.8 |  | 0.9 | 0.2 | 6.8 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 19.7 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\stackrel{\square}{1}$ |  | \％ | $\uparrow$ | F | \％ | $\uparrow$ | F | \％ | 个t |  |
| Trafic Volume（veh／h） | 42 | 32 | 23 | 142 | 40 | 312 | 40 | 713 | 130 | 296 | 828 | 29 |
| Future Volume（veh／h） | 42 | 32 | 23 | 142 | 40 | 312 | 40 | 713 | 130 | 296 | 828 | 29 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／n | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1945 | 1945 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 42 | 32 | 23 | 142 | 40 | 312 | 40 | 713 | 130 | 296 | 828 | 29 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 54 | 51 | 36 | 136 | 178 | 720 | 55 | 715 | 606 | 640 | 2489 | 87 |
| Arrive On Green | 0.03 | 0.05 | 0.05 | 0.08 | 0.10 | 0.10 | 0.03 | 0.37 | 0.37 | 0.72 | 1.00 | 1.00 |
| Sat Flow，veh／h | 1781 | 1012 | 727 | 1781 | 1870 | 1585 | 1781 | 1945 | 1648 | 1781 | 3502 | 123 |
| Grp Volume（v）veh／h | 42 | 0 | 55 | 142 | 40 | 312 | 40 | 713 | 130 | 296 | 420 | 437 |
| Grp Sat Flow（s），veh／h／nn | 1781 | 0 | 1739 | 1781 | 1870 | 1585 | 1781 | 1945 | 1648 | 1781 | 1777 | 1848 |
| Q Serve（g＿s），s | 2.8 | 0.0 | 3.7 | 9.0 | 2.3 | 1.9 | 2.6 | 43.2 | 6.4 | 8.3 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 2.8 | 0.0 | 3.7 | 9.0 | 2.3 | 1.9 | 2.6 | 43.2 | 6.4 | 8.3 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.42 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.07 |
| Lane Grp Cap（c），veh／h | 54 | 0 | 87 | 136 | 178 | 720 | 55 | 715 | 606 | 640 | 1263 | 1314 |
| V／C Ratio（X） | 0.78 | 0.00 | 0.63 | 1.05 | 0.22 | 0.43 | 0.73 | 1.00 | 0.21 | 0.46 | 0.33 | 0.33 |
| Avail Cap（c＿a），veh／h | 106 | 0 | 457 | 136 | 523 | 1013 | 106 | 715 | 606 | 640 | 1263 | 1314 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.79 | 0.79 | 0.79 |
| Uniform Delay（d），s／veh | 56.8 | 0.0 | 55.0 | 54.5 | 49.4 | 12.5 | 56.7 | 37.2 | 25.6 | 11.8 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 21.1 | 0.0 | 7.4 | 89.8 | 0.6 | 0.4 | 6.6 | 32.8 | 0.8 | 0.2 | 0.6 | 0.5 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（ $50 \%$ ），veh／ | \11． 6 | 0.0 | 1.8 | 7.4 | 1.1 | 4.1 | 1.3 | 26.1 | 2.6 | 2.5 | 0.2 | 0.2 |
| Unsig．Movement Delay， | ，s／veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 77.9 | 0.0 | 62.4 | 144.3 | 50.0 | 12.9 | 63.3 | 70.1 | 26.4 | 11.9 | 0.6 | 0.5 |
| LnGrp LOS | E | A | E | F | D | B | E | E | C | B | A | A |
| Approach Vol，veh／h |  | 97 |  |  | 494 |  |  | 883 |  |  | 1153 |  |
| Approach Delay，s／veh |  | 69.1 |  |  | 53.7 |  |  | 63.3 |  |  | 3.5 |  |
| Approach LOS |  | E |  |  | D |  |  | E |  |  | A |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， | ， 4.1 | 48.1 | 13.0 | 9.8 | 6.7 | 88.6 | 7.6 | 15.2 |  |  |  |  |
| Change Period（ $Y+R \mathrm{Cc}$ ）， s | s 4.7 | ＊ 4.7 | 4.0 | 3.9 | 3.0 | 4.7 | 4.0 | ＊4 |  |  |  |  |
| Max Green Setting（Gma | ake， 3 | ＊ 43 | 9.0 | 31.0 | 7.0 | 55.4 | 7.0 | ＊ 33 |  |  |  |  |
| Max Q Clear Time（g＿c＋1 | ＋ 119 | 45.2 | 11.0 | 5.7 | 4.6 | 2.0 | 4.8 | 4.3 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.3 | 0.0 | 0.0 | 0.2 | 0.0 | 5.9 | 0.0 | 1.3 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 35.5 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

[^4]
## PM Baseline

Stony Oaks TIS



| HCM 6th Signalized Intersection Summary <br> 5: Hearn Ave \& Dutton Meadow |  |  |  |  |  |  |  |  |  |  | 02/11/2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{ }$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{}$ |  | \% | $\uparrow$ |  |  | $\uparrow$ | * |  |  |  |
| Traffic Volume (veh/h) | 0 | 444 | 89 | 289 | 636 | 0 | 128 | 0 | 314 | 0 | 0 | 0 |
| Future Volume (veh/h) | 0 | 444 | 89 | 289 | 636 | 0 | 128 | 0 | 314 | 0 | 0 | 0 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1870 | 1870 | 1870 | 1870 | 0 | 1870 | 1870 | 1870 |  |  |  |
| Adj Flow Rate, veh/h | 0 | 444 | 89 | 289 | 636 | 0 | 128 | 0 | 314 |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Percent Heavy Veh, \% | 0 | 2 | 2 | 2 | 2 | 0 | 2 | 2 | 2 |  |  |  |
| Cap, veh/h | 0 | 567 | 114 | 357 | 1243 | 0 | 307 | 0 | 591 |  |  |  |
| Arrive On Green | 0.00 | 0.37 | 0.37 | 0.20 | 0.66 | 0.00 | 0.17 | 0.00 | 0.17 |  |  |  |
| Sat Flow, veh/h | 0 | 1513 | 303 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Grp Volume(v), veh/h | 0 | 0 | 533 | 289 | 636 | 0 | 128 | 0 | 314 |  |  |  |
| Grp Sat Flow(s),veh/h/n | 0 | 0 | 1816 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Q Serve(g_s), s | 0.0 | 0.0 | 10.5 | 6.3 | 7.0 | 0.0 | 2.6 | 0.0 | 0.0 |  |  |  |
| Cycle Q Clear (__c), s | 0.0 | 0.0 | 10.5 | 6.3 | 7.0 | 0.0 | 2.6 | 0.0 | 0.0 |  |  |  |
| Prop In Lane | 0.00 |  | 0.17 | 1.00 |  | 0.00 | 1.00 |  | 1.00 |  |  |  |
| Lane $\operatorname{Grp} \operatorname{Cap}(\mathrm{c})$, veh/h | 0 | 0 | 681 | 357 | 1243 | 0 | 307 | 0 | 591 |  |  |  |
| V/C Ratio(X) | 0.00 | 0.00 | 0.78 | 0.81 | 0.51 | 0.00 | 0.42 | 0.00 | 0.53 |  |  |  |
| Avail Cap(c_a), veh/h | 0 | 0 | 1052 | 529 | 1779 | 0 | 794 | 0 | 1024 |  |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter(l) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |  |  |  |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 11.2 | 15.4 | 3.4 | 0.0 | 14.9 | 0.0 | 9.9 |  |  |  |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 2.1 | 3.4 | 0.3 | 0.0 | 0.9 | 0.0 | 0.7 |  |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \%ile BackOfQ(50\%),veh/n | 0.0 | 0.0 | 3.5 | 2.4 | 1.0 | 0.0 | 0.9 | 0.0 | 1.6 |  |  |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 0.0 | 0.0 | 13.3 | 18.8 | 3.8 | 0.0 | 15.8 | 0.0 | 10.7 |  |  |  |
| LnGrp LOS | A | A | B | B | A | A | B | A | B |  |  |  |
| Approach Vol, veh/h |  | 533 |  |  | 925 |  |  | 442 |  |  |  |  |
| Approach Delay, s/veh |  | 13.3 |  |  | 8.5 |  |  | 12.1 |  |  |  |  |
| Approach LOS |  | B |  |  | A |  |  | B |  |  |  |  |
| Timer - Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 11.7 | 18.7 |  |  |  | 30.4 |  | 10.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.6 | * 3.6 |  |  |  | 3.6 |  | 3.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 12.0 | *23 |  |  |  | 38.4 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 8.3 | 12.5 |  |  |  | 9.0 |  | 4.6 |  |  |  |  |
| Green Ext Time (p_c), s | 0.2 | 2.6 |  |  |  | 4.8 |  | 1.5 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 10.7 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| HCM 6th Signalized Intersection Summary <br> 1：Stony Point Rd \＆Northpoint Pkwy |  |  |  |  |  |  |  |  |  |  | 02／03／2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\Rightarrow$ | $\rightarrow$ | 7 | $t$ | $\leftarrow$ |  | 4 | $\dagger$ | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ |  | F |  |  |  | \％ | 个的 |  | \％ | 个家 |  |
| Traffic Volume（veh／h） | 58 | 0 | 189 | 0 | 0 | 0 | 392 | 824 | 0 | 0 | 824 | 116 |
| Future Volume（veh／h） | 58 | 0 | 189 | 0 | 0 | 0 | 392 | 824 | 0 | 0 | 824 | 116 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 0 | 1870 |  |  |  | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 58 | 0 | 189 |  |  |  | 392 | 824 | 0 | 0 | 824 | 116 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 0 | 2 |  |  |  | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 228 | 0 | 341 |  |  |  | 561 | 2830 | 0 | 67 | 2130 | 300 |
| Arrive On Green | 0.13 | 0.00 | 0.13 |  |  |  | 0.12 | 1.00 | 0.00 | 0.00 | 0.68 | 0.68 |
| Sat Flow，veh／h | 1781 | 0 | 1585 |  |  |  | 1781 | 3647 | 0 | 665 | 3128 | 440 |
| Grp Volume（v），veh／h | 58 | 0 | 189 |  |  |  | 392 | 824 | 0 | 0 | 468 | 472 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1585 |  |  |  | 1781 | 1777 | 0 | 665 | 1777 | 1791 |
| Q Serve（g＿s），s | 3.2 | 0.0 | 11.5 |  |  |  | 6.9 | 0.0 | 0.0 | 0.0 | 12.3 | 12.3 |
| Cycle Q Clear（g＿c），s | 3.2 | 0.0 | 11.5 |  |  |  | 6.9 | 0.0 | 0.0 | 0.0 | 12.3 | 12.3 |
| Prop In Lane | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.00 | 1.00 |  | 0.25 |
| Lane Grp Cap（c），veh／h | 228 | 0 | 341 |  |  |  | 561 | 2830 | 0 | 67 | 1210 | 1220 |
| VIC Ratio（X） | 0.25 | 0.00 | 0.55 |  |  |  | 0.70 | 0.29 | 0.00 | 0.00 | 0.39 | 0.39 |
| Avail Cap（c＿a），veh／h | 463 | 0 | 551 |  |  |  | 883 | 2830 | 0 | 67 | 1210 | 1220 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  |  |  | 1.33 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 0.00 | 1.00 |  |  |  | 0.77 | 0.77 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 42.5 | 0.0 | 37.7 |  |  |  | 5.6 | 0.0 | 0.0 | 0.0 | 7.5 | 7.5 |
| Incr Delay（d2），s／veh | 0.2 | 0.0 | 0.5 |  |  |  | 0.5 | 0.2 | 0.0 | 0.0 | 0.9 | 0.9 |
| Initial Q Delay（d3），S／veh | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.4 | 0.0 | 10.2 |  |  |  | 1.5 | 0.1 | 0.0 | 0.0 | 4.3 | 4.3 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 42.7 | 0.0 | 38.3 |  |  |  | 6.1 | 0.2 | 0.0 | 0.0 | 8.4 | 8.4 |
| LnGrp LOS | D | A | D |  |  |  | A | A | A | A | A | A |
| Approach Vol，veh／h |  | 247 |  |  |  |  |  | 1216 |  |  | 940 |  |
| Approach Delay，s／veh |  | 39.3 |  |  |  |  |  | 2.1 |  |  | 8.4 |  |
| Approach LOS |  | D |  |  |  |  |  | A |  |  | A |  |
| Timer－Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{C})$ ，$s$ |  | 89.9 |  | 18.1 | 12.5 | 77.4 |  |  |  |  |  |  |
| Change Period（ $Y+R \mathrm{c}$ ），$s$ |  | 3.9 |  | 4.3 | 3.0 | 3.9 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | 71.7 |  | 28.1 | 29.0 | 39.7 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  | 13.5 | 8.9 | 14.3 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 6.5 |  | 0.3 | 0.5 | 6.2 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 8.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | A |  |  |  |  |  |  |  |  |  |


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| :--- | ---: |
| Stony Oaks TIS | Page 1 |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | f |  | \％ | $\uparrow$ | 「 | $\dagger$ | $\uparrow$ | 7 | \％ | $\uparrow \uparrow$ |  |
| Traffic Volume（veh／h） | 117 | 61 | 47 | 95 | 18 | 326 | 9 | 555 | 71 | 262 | 711 |  |
| Future Volume（veh／h） | 117 | 61 | 47 | 95 | 18 | 326 | 9 | 555 | 71 | 262 | 711 |  |

Future Volume（veh／h） $11 \begin{array}{llllllllllll}117 & 61 & 47 & 95 & 18 & 326 & 9 & 555 & 71 & 262 & 711 & 10\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Initial Q（Qb），veh } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \text { Ped－Bike Adj（A＿pbT）} & 1.00 & 1.00 & 1.00 & & 1.00 & 1.00 & & 1.00 & 1.00 & & 1.00\end{array}$
$\begin{array}{llllllllllllll}\text { Parking Bus，Adj } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$
$\begin{array}{lllllllllllllll}\text { Work Zone On Approach } & \text { No } & & & \text { No } & & & \text { No } & & & \text { No } \\ \text { Adj Sat Flow，veh／h／n } & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1945 & 1945 & 1870 & 1870 & 1870\end{array}$
$\begin{array}{llllllllrrrrr}\text { Adj Flow Rate，veh／h } & 117 & 61 & 47 & 95 & 18 & 326 & 9 & 555 & 71 & 262 & 711 & 16\end{array}$

$\begin{array}{lrrrrrrrrrrr}\text { Percent Heavy Veh，\％} & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Cap，veh／h } & 132 & 161 & 124 & 120 & 297 & 513 & 316 & 891 & 755 & 293 & 1526 & 34 \\ \text { Arrive On Green } & 0.07 & 0.16 & 0.16 & 0.07 & 0.16 & 0.16 & 0.18 & 0.46 & 0.46 & 0.05 & 0.14 & 0.14\end{array}$
$\begin{array}{lllllllllllll}\text { Arrive On Green } & 0.07 & 0.16 & 0.16 & 0.07 & 0.16 & 0.16 & 0.18 & 0.46 & 0.46 & 0.05 & 0.14 & 0.14 \\ \text { Sat Flow，veh／h } & 1781 & 980 & 755 & 1781 & 1870 & 1585 & 1781 & 1945 & 1648 & 1781 & 3553 & 8\end{array}$

| Sat |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Grp Volume（v），veh／h | 117 | 0 | 108 | 95 | 18 | 326 | 9 | 555 | 71 | 262 | 355 | 372 |

Grp Sat Flow（s），veh／h／lin1781 $\begin{array}{llllllllllll} & 0 & 1734 & 1781 & 1870 & 1585 & 1781 & 1945 & 1648 & 1781 & 1777 & 1856\end{array}$
$\begin{array}{lllllllllllll}\text { Q Serve }\left(g \_s\right), ~ s ~ & 7.0 & 0.0 & 6.0 & 5.7 & 0.9 & 14.0 & 0.5 & 23.4 & 2.6 & 15.8 & 19.9 & 19.9\end{array}$
$\begin{array}{lllllllllllll}\text { Cycle Q Clear（g＿c），s } & 7.0 & 0.0 & 6.0 & 5.7 & 0.9 & 14.0 & 0.5 & 23.4 & 2.6 & 15.8 & 19.9 & 19.9\end{array}$

| Prop In Lane | 1.00 | 0.44 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

$\begin{array}{lllllllllllll}\text { Lane Grp Cap（c），veh／h } & 132 & 0 & 286 & 120 & 297 & 513 & 316 & 891 & 755 & 293 & 763 & 79\end{array}$
$\begin{array}{lllllllllllll}\text { V／C Ratio（X）} & 0.89 & 0.00 & 0.38 & 0.79 & 0.06 & 0.64 & 0.03 & 0.62 & 0.09 & 0.89 & 0.47 & 0.47\end{array}$
$\begin{array}{lllllllllllll}\text { Avail Cap（c＿a），veh／h } & 132 & 0 & 514 & 148 & 571 & 745 & 316 & 891 & 755 & 297 & 763 & 797\end{array}$
Unstream Filter（I）$\quad 100 \quad 0.00 \quad 100$
Uniform Delay（d）s／veh 49．6 $\begin{array}{lllllllllllll} & 0.0 & 40.2 & 49.6 & 38.6 & 17.9 & 36.7 & 22.2 & 16.6 & 50.1 & 350 & 35.0\end{array}$
$\begin{array}{lllllllllllll}\text { Incr Delay（d2），s／veh } & 46.1 & 0.0 & 0.8 & 20.7 & 0.1 & 1.3 & 0.0 & 3.3 & 0.2 & 24.3 & 1.9 & 1.8\end{array}$
$\begin{array}{llllllllllllll}\text { Incr Delay（d2），slveh } & 46.1 & 0.0 & 0.8 & 20.7 & 0.1 & 1.3 & 0.0 & 3.3 & 0.2 & 24.3 & 1.9 & 1.8 \\ \text { Initial Q Delay（d3），s／veh } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0\end{array}$
$\begin{array}{llllllllllll}\text { \％ile BackOfQ（ } 50 \% \text { ），veh／rf．} 8 & 0.0 & 2.6 & 3.2 & 0.4 & 5.2 & 0.2 & 10.9 & 1.0 & 9.5 & 9.8 & 10.2\end{array}$
Unsig．Movement Delay，s／veh



|  | A |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
|  | 225 | 439 | 635 | 989 |  |
| Appproach Vol，veh／h | 69.4 | 31.1 | 24.7 | 46.7 |  |


| Approach Delay，slveh | 69.4 | E | 31.1 | 24.7 |
| :--- | ---: | ---: | ---: | ---: |
| Approach LOS | E | C | 46.7 |  |

$\begin{array}{llllllllll}\text { Approach LOS } & & \text { E } & & & \text { C } & & & \text { C }\end{array}$

Change Period（Y＋Rc），s 3.0 4．7 4.0 ＊4 4.7 ＊4．7 4.0
$\begin{array}{llllllll}\text { Max Green Setting（Gmaxp，00 } & 33.4 & 9.0 & * 32 & 5.0 & * 46 & 8.0 & 33.0\end{array}$
$\begin{array}{lrrrrrrr}\text { Max Q Clear Time（g＿c }+ \text { HITI，} 8 & 25.4 & 7.7 & 8.0 & 2.5 & 21.9 & 9.0 & 16.0 \\ \text { Green Ext Time（p＿c），} & 0.0 & 2.3 & 0.0 & 0.5 & 0.0 & 4.3 & 0.0 \\ 1.1\end{array}$
Intersection Summary

## HCM 6th Ctrl Delay

HCM 6th LOS
39.8
＊HCM 6 th computational engine requires equal clearance times for the phases crossing the barrier


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| :--- | ---: |
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| HCM 6th Signalized Intersection Summary <br> 5: Hearn Ave \& Dutton Meadow |  |  |  |  |  |  |  |  |  |  | 02/03/2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{ }$ | $\rightarrow$ | 7 | $\checkmark$ | $\longleftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\downarrow$ | $\downarrow$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{}$ |  | \% | $\uparrow$ |  |  | $\uparrow$ | F |  |  |  |
| Traffic Volume (veh/h) | 0 | 524 | 64 | 367 | 438 | 0 | 102 | 0 | 406 | 0 | 0 | 0 |
| Future Volume (veh/h) | 0 | 524 | 64 | 367 | 438 | 0 | 102 | 0 | 406 | 0 | 0 | 0 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1870 | 1870 | 1870 | 1870 | 0 | 1870 | 1870 | 1870 |  |  |  |
| Adj Flow Rate, veh/h | 0 | 524 | 64 | 367 | 438 | 0 | 102 | 0 | 406 |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Percent Heavy Veh, \% | 0 | 2 | 2 | 2 | 2 | 0 | 2 | 2 | 2 |  |  |  |
| Cap, veh/h | 0 | 623 | 76 | 426 | 1309 | 0 | 275 | 0 | 624 |  |  |  |
| Arrive On Green | 0.00 | 0.38 | 0.38 | 0.24 | 0.70 | 0.00 | 0.15 | 0.00 | 0.15 |  |  |  |
| Sat Flow, veh/h | 0 | 1635 | 200 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Grp Volume(v), veh/h | 0 | 0 | 588 | 367 | 438 | 0 | 102 | 0 | 406 |  |  |  |
| Grp Sat Flow(s),veh/h/n | 0 | 0 | 1834 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Q Serve(g_s), s | 0.0 | 0.0 | 13.2 | 8.9 | 4.2 | 0.0 | 2.3 | 0.0 | 0.0 |  |  |  |
| Cycle Q Clear (__c), s | 0.0 | 0.0 | 13.2 | 8.9 | 4.2 | 0.0 | 2.3 | 0.0 | 0.0 |  |  |  |
| Prop In Lane | 0.00 |  | 0.11 | 1.00 |  | 0.00 | 1.00 |  | 1.00 |  |  |  |
| Lane $\operatorname{Grp} \operatorname{Cap}(\mathrm{c})$, veh/h | 0 | 0 | 699 | 426 | 1309 | 0 | 275 | 0 | 624 |  |  |  |
| V/C Ratio(X) | 0.00 | 0.00 | 0.84 | 0.86 | 0.33 | 0.00 | 0.37 | 0.00 | 0.65 |  |  |  |
| Avail Cap(c_a), veh/h | 0 | 0 | 867 | 433 | 1463 | 0 | 708 | 0 | 1010 |  |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter(l) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |  |  |  |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 12.8 | 16.5 | 2.7 | 0.0 | 17.2 | 0.0 | 11.2 |  |  |  |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 6.2 | 15.2 | 0.1 | 0.0 | 0.8 | 0.0 | 1.2 |  |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \%ile BackOfQ(50\%),veh/n | 0.0 | 0.0 | 5.5 | 4.9 | 0.6 | 0.0 | 0.9 | 0.0 | 2.7 |  |  |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 0.0 | 0.0 | 19.0 | 31.7 | 2.8 | 0.0 | 18.0 | 0.0 | 12.3 |  |  |  |
| LnGrp LOS | A | A | B | C | A | A | B | A | B |  |  |  |
| Approach Vol, veh/h |  | 588 |  |  | 805 |  |  | 508 |  |  |  |  |
| Approach Delay, s/veh |  | 19.0 |  |  | 16.0 |  |  | 13.5 |  |  |  |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  |  |  |
| Timer - Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 14.4 | 20.8 |  |  |  | 35.3 |  | 10.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.6 | *3.6 |  |  |  | 3.6 |  | 3.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 11.0 | *21 |  |  |  | 35.4 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 10.9 | 15.2 |  |  |  | 6.2 |  | 4.3 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 2.0 |  |  |  | 2.9 |  | 1.7 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 16.2 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

HCM 6 th computational engine requires equal clearance times for the phases crossing the barrier.

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| :--- | ---: |
| Stony Oaks TIS | Page 5 |


| HCM 6th Signalized Intersection Summary 1：Stony Point Rd \＆Northpoint Pkwy |  |  |  |  |  |  |  |  |  |  | 02／03／2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\Rightarrow$ |  | $\nu$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | P | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ |  | F |  |  |  | ＊ | 个家 |  | \％ | 个家 |  |
| Traffic Volume（veh／h） | 130 | 0 | 422 | 0 | 0 | 0 | 169 | 795 | 0 | 0 | 949 | 43 |
| Future Volume（veh／h） | 130 | 0 | 422 | 0 | 0 | 0 | 169 | 795 | 0 | 0 | 949 | 43 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 0 | 1870 |  |  |  | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 130 | 0 | 422 |  |  |  | 169 | 795 | 0 | 0 | 949 | 43 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 0 | 2 |  |  |  | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 171 | 0 | 736 |  |  |  | 832 | 2966 | 0 | 61 | 1499 | 68 |
| Arrive On Green | 0.10 | 0.00 | 0.10 |  |  |  | 0.74 | 1.00 | 0.00 | 0.00 | 0.43 | 0.43 |
| Sat Flow，veh／h | 1781 | 0 | 1585 |  |  |  | 1781 | 3647 | 0 | 683 | 3462 | 157 |
| Grp Volume（v），veh／h | 130 | 0 | 422 |  |  |  | 169 | 795 | 0 | 0 | 487 | 505 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1585 |  |  |  | 1781 | 1777 | 0 | 683 | 1777 | 1842 |
| Q Serve（g＿s），s | 8.4 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 25.3 | 25.3 |
| Cycle Q Clear（g＿c），s | 8.4 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 25.3 | 25.3 |
| Prop In Lane | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.00 | 1.00 |  | 0.09 |
| Lane Grp Cap（c），veh／h | 171 | 0 | 736 |  |  |  | 832 | 2966 | 0 | 61 | 769 | 798 |
| V／C Ratio（X） | 0.76 | 0.00 | 0.57 |  |  |  | 0.20 | 0.27 | 0.00 | 0.00 | 0.63 | 0.63 |
| Avail Cap（c＿a），veh／h | 433 | 0 | 970 |  |  |  | 832 | 2966 | 0 | 61 | 769 | 798 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  |  |  | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 |  |  |  | 0.79 | 0.79 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 52.0 | 0.0 | 23.1 |  |  |  | 5.2 | 0.0 | 0.0 | 0.0 | 26.1 | 26.1 |
| Incr Delay（d2），s／veh | 2.6 | 0.0 | 0.3 |  |  |  | 0.0 | 0.2 | 0.0 | 0.0 | 3.9 | 3.8 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／n | 3.8 | 0.0 | 13.9 |  |  |  | 0.9 | 0.1 | 0.0 | 0.0 | 11.1 | 11.4 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 54.7 | 0.0 | 23.3 |  |  |  | 5.2 | 0.2 | 0.0 | 0.0 | 30.1 | 29.9 |
| LnGrp LOS | D | A | C |  |  |  | A | A | A | A | C | C |
| Approach Vol，veh／h |  | 552 |  |  |  |  |  | 964 |  |  | 992 |  |
| Approach Delay，s／veh |  | 30.7 |  |  |  |  |  | 1.1 |  |  | 30.0 |  |
| Approach LOS |  | C |  |  |  |  |  | A |  |  | C |  |
| Timer－Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s |  | 102.4 |  | 15.6 | 47.4 | 55.0 |  |  |  |  |  |  |
| Change Period（ $Y+R \mathrm{C}$ ），s |  | 3.9 |  | 4.3 | 3.9 | ＊ 3.9 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | 81.1 |  | 28.7 | 27.0 | ＊51 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s |  | 2.0 |  | 10.4 | 2.0 | 27.3 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 6.2 |  | 0.9 | 0.2 | 6.4 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 19.0 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

# Movement EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT 


$\begin{array}{lllllllllllll}\text { Traffic Volume（veh／h）} & 42 & 22 & 23 & 121 & 34 & 296 & 40 & 672 & 122 & 268 & 775 & 29\end{array}$ $\begin{array}{lrrrrrrrrrrrr}\text { Initial Q（Qb），veh } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$ $\begin{array}{lllllllllllll}\text { Parking Bus，Adj } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$
$\begin{array}{lllllllll}\text { Work Zone On Approach } & \text { No } & & \text { No } & & \text { No } & & \text { No }\end{array}$
Adj Sat Flow，veh／h／ln 1870187018701870187018701870
$\begin{array}{lrrrrrrrrrrrr}\text { Adj Flow Rate，veh／h } & 42 & 22 & 23 & 121 & 34 & 296 & 40 & 672 & 122 & 268 & 775 & 29\end{array}$
$\begin{array}{lllllllllllll}\text { Peak Hour Factor } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$
$\begin{array}{llllllllllllll}\text { Cap，veh／h } & 54 & 37 & 39 & 136 & 167 & 720 & 55 & 715 & 606 & 650 & 2502 & 94\end{array}$

$\begin{array}{lrrrrrrrrrrrr}\text { Cap，veh／h } & 54 & 37 & 39 & 136 & 167 & 720 & 55 & 715 & 606 & 650 & 2502 & 9 . \\ \text { Arrive On Green } & 0.03 & 0.04 & 0.04 & 0.08 & 0.09 & 0.09 & 0.03 & 0.37 & 0.37 & 0.73 & 1.00 & 1.00\end{array}$ | Arrive On Green | 0.03 | 0.04 | 0.04 | 0.08 | 0.09 | 0.09 | 0.03 | 0.37 | 0.37 | 0.73 | 1.00 | 1.00 |
| :--- | ---: | :--- | :--- | :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Sat Flow，veh／h | 1781 | 837 | 875 | 1781 | 1870 | 1585 | 1781 | 1945 | 1648 | 1781 | 3493 | 131 | $\begin{array}{lllllllllllll}\text { Grp Volume（v），veh／h } & 42 & 0 & 45 & 121 & 34 & 296 & 40 & 672 & 122 & 268 & 394 & 410\end{array}$


$\begin{array}{lllllllllllll}\text { Q Serve（g＿s），s } & 2.8 & 0.0 & 3.0 & 7.9 & 2.0 & 1.7 & 2.6 & 39.4 & 6.0 & 6.9 & 0.0 & 0.0\end{array}$ $\begin{array}{lllllllllllll}\text { Cycle Q Clear（g＿c），s } & 2.8 & 0.0 & 3.0 & 7.9 & 2.0 & 1.7 & 2.6 & 39.4 & 6.0 & 6.9 & 0.0 & 0.0\end{array}$ $\begin{array}{llllllllll}\text { Prop In Lane } & 1.00 & 0.51 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 0.07\end{array}$ $\begin{array}{lllllllllllll}\text { Lane } \operatorname{Grp} \mathrm{Cap}(\mathrm{c}) \text { ，veh／h } & 54 & 0 & 76 & 136 & 167 & 720 & 55 & 715 & 606 & 650 & 1273 & 1323\end{array}$ $\begin{array}{lllllllllllll}\text { V／C Ratio（X）} & 0.78 & 0.00 & 0.59 & 0.89 & 0.20 & 0.41 & 0.73 & 0.94 & 0.20 & 0.41 & 0.31 & 0.3\end{array}$ $\begin{array}{lllllllllllll}\text { Avail Cap（c＿a），veh／h } & 106 & 0 & 450 & 136 & 523 & 1022 & 106 & 715 & 606 & 650 & 1273 & 132\end{array}$ Unstream Filter（l） $\begin{array}{lllllllllllll} & 1.00 & 0.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 0.81 & 0.81 & 0.81\end{array}$ $\begin{array}{lllllllllllll}\text { Uniform Delay（d）．s／veh 56．8 } & 0.0 & 55.4 & 54.0 & 49.8 & 12.4 & 56.7 & 36.0 & 25.5 & 11.0 & 0.0 & 0.0\end{array}$
$\begin{array}{lllllllllllll}\text { Incr Delay（d2），s／veh } & 21.1 & 0.0 & 7.2 & 46.1 & 0.6 & 0.4 & 6.6 & 21.7 & 0.7 & 0.1 & 0.5 & 0.5\end{array}$
$\begin{array}{lllllllllllll}\text { Incr Delay（d2），slveh } & 21.1 & 0.0 & 7.2 & 46.1 & 0.6 & 0.4 & 6.6 & 21.7 & 0.7 & 0.1 & 0.5 & 0.5 \\ \text { Initial Q Delay（d3），s／veh } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0\end{array}$
$\begin{array}{llllllllllll}\text { \％ile BackOfQ（ } 50 \% \text { ），veh／r1．} 6 & 0.0 & 1.5 & 5.3 & 1.0 & 3.9 & 1.3 & 22.2 & 2.5 & 2.1 & 0.2 & 0.2\end{array}$
Unsig．Movement Delay，s／veh
$\left.\begin{array}{lllllllllllllll}\text { LnGrp Delay（d），S／veh } & 77.9 & 0.0 & 62.6 & 100.1 & 50.4 & 12.7 & 63.3 & 57.7 & 26.2 & 11.2 & 0.5 & 0.5\end{array}\right]$


|  |  |  |  | A |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Approach Vol，veh／h | 87 | 451 | 834 | 1072 |
| Approach Delay，slveh | 70.0 | 39.0 | 53.4 | 3.2 |
| Approach LOS |  |  |  |  |


| Approach Delay，s／veh | 70.0 | 39.0 | 53.4 | 3.2 |
| :--- | :---: | :---: | :---: | :---: |
| Approach LOS | E | D | D | A |

$\begin{array}{lrrrrrrrr}\text { Timer－Assigned Phs } & 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8\end{array}$
$\begin{array}{llllllll}\text { Phs Duration }(G+Y+R c), 47.8 & 48.1 & 13.0 & 9.1 & 6.7 & 89.2 & 7.6 & 14.6\end{array}$
Change Period $(Y+R c)$ ，s 4.7 ＊ 4.7 4．0 3.9 3．9 3.0
$\begin{array}{lllllllll}\text { Max Green Setting（Gmax9，0 } & \text {＊} 43 & 9.0 & 31.0 & 7.0 & 55.4 & 7.0 & & * 33\end{array}$
$\begin{array}{lrllllll}\text { Max Q Clear Time（g＿c } \mathrm{c} 188,9 & 41.4 & 9.9 & 5.0 & 4.6 & 2.0 & 4.8 & 4.0 \\ \text { Green Ext Time（p＿c），s } & 0.3 & 1.0 & 0.0 & 0.2 & 0.0 & 5.4 & 0.0 \\ 1.2\end{array}$

## Intersection Summary

## HCM 6 th Ctrl Delay

HCM
29.3
$C$
${ }^{*}$ NCM NCM 6 th computational engine requires equal clearance times for the phases crossing the barrier．




| PM Existing Plus Project | Synchro 11 Report |
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| Stony Oaks TIS | Page 5 |

HCM 6th Signalized Intersection Summary
1: Stony Point Rd \& Northpoint Pkwy

|  | $\Rightarrow$ |  |  |  |  |  | 4 | $\uparrow$ | $P$ | * | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 9 |  | 7 |  |  |  | \% | 个t |  | \% | 个t |  |
| Traffic Volume (veh/h) | 58 | 0 | 195 | 0 | 0 | 0 | 397 | 915 | 0 | 0 | 862 | 116 |
| Future Volume (veh/h) | 58 | 0 | 195 | 0 | 0 | 0 | 397 | 915 | 0 | 0 | 862 | 116 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 0 | 1870 |  |  |  | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 58 | 0 | 195 |  |  |  | 397 | 915 | 0 | 0 | 862 | 116 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 2 | 0 | 2 |  |  |  | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 233 | 0 | 350 |  |  |  | 545 | 2818 | 0 | 67 | 2126 | 286 |
| Arrive On Green | 0.13 | 0.00 | 0.13 |  |  |  | 0.12 | 1.00 | 0.00 | 0.00 | 0.68 | 0.68 |
| Sat Flow, veh/h | 1781 | 0 | 1585 |  |  |  | 1781 | 3647 | 0 | 610 | 3147 | 424 |
| Grp Volume(v), veh/h | 58 | 0 | 195 |  |  |  | 397 | 915 | 0 | 0 | 487 | 491 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1585 |  |  |  | 1781 | 1777 | 0 | 610 | 1777 | 1794 |
| Q Serve(g_s), s | 3.2 | 0.0 | 11.8 |  |  |  | 7.2 | 0.0 | 0.0 | 0.0 | 13.2 | 13.2 |
| Cycle Q Clear(g_c), s | 3.2 | 0.0 | 11.8 |  |  |  | 7.2 | 0.0 | 0.0 | 0.0 | 13.2 | 13.2 |
| Prop In Lane | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.00 | 1.00 |  | 0.24 |
| Lane Grp Cap(c), veh/h | 233 | 0 | 350 |  |  |  | 545 | 2818 | 0 | 67 | 1200 | 1212 |
| V/C Ratio(X) | 0.25 | 0.00 | 0.56 |  |  |  | 0.73 | 0.32 | 0.00 | 0.00 | 0.41 | 0.41 |
| Avail Cap(c_a), veh/h | 463 | 0 | 555 |  |  |  | 863 | 2818 | 0 | 67 | 1200 | 1212 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  |  |  | 1.33 | 1.33 | 1.33 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 |  |  |  | 0.70 | 0.70 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 42.2 | 0.0 | 37.4 |  |  |  | 6.3 | 0.0 | 0.0 | 0.0 | 7.8 | 7.8 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 0.5 |  |  |  | 0.5 | 0.2 | 0.0 | 0.0 | 1.0 | 1.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.4 | 0.0 | 10.5 |  |  |  | 1.6 | 0.1 | 0.0 | 0.0 | 4.6 | 4.7 |



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| :--- | ---: |
| Stony Oaks TIS | Page 1 |




$\begin{array}{lllllllllllll}\text { Trafic Volume (venh } \\ \text { Future Volume (veh/h) } & 117 & 64 & 47 & 106 & 27 & 359 & 9 & 618 & 95 & 285 & 732 & 16\end{array}$ $\begin{array}{lrrrrrrrrrrrr}\text { Initial Q (Qb), veh } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \text { Ped-Bike Adj(A_pbT) } & 1.00 & & 1.00 & 1.00 & & 1.00 & 1.00 & & 1.00 & 1.00 & & 1.00\end{array}$ $\begin{array}{llllllllllllll}\text { Parking Bus, Adj } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$ $\begin{array}{lllllllllllllll}\text { Work Zone On Approach } & \text { No } & & & \text { No } & & & \text { No } & & & \text { No } \\ \text { Adj Sat Flow, veh/h/n } & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1945 & 1945 & 1870 & 1870 & 1870\end{array}$ $\begin{array}{lrrrrrrrrrrrr}\text { Adj Sat Flow, veh/h/n } & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1870 & 1945 & 1945 & 1870 & 1870 & 1870 \\ \text { Adj Flow Rate, veh/h } & 117 & 64 & 47 & 106 & 27 & 359 & 9 & 618 & 95 & 285 & 732 & 16\end{array}$

$\begin{array}{lrrrrrrrrrrrr}\text { Adj Flow Rate, veh/h } & 117 & 64 & 47 & 106 & 27 & 359 & 9 & 618 & 95 & 285 & 732 & 16 \\ \text { Peak Hour Factor } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$ $\begin{array}{lrrrrrrrrrrrr}\text { Peak Hour Factor } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 \\ \text { Percent Heavy Veh, \% } & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2\end{array}$ $\begin{array}{lrrrrrrrrrrrr}\text { Percent Heavy Ven, } \% & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 \\ \text { Cap, veh/h } & 132 & 172 & 126 & 132 & 323 & 538 & 291 & 860 & 729 & 297 & 1528 & 33\end{array}$ $\begin{array}{lrlllllllllll}\text { Arrive On Green } & 0.07 & 0.17 & 0.17 & 0.07 & 0.17 & 0.17 & 0.16 & 0.44 & 0.44 & 0.00 & 0.14 & 0.14\end{array}$ |  | 1781 | 1002 | 736 | 1781 | 1870 | 1585 | 1781 | 1945 | 1648 | 1781 | 3556 | 7 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Grp Volume(v) veh/h | 117 | 0 | 111 | 106 | 2 | 35 |  | 618 | 95 | 285 | 366 |  | 38 | $\begin{array}{lllllllllllllll}\text { Grp Sat Flow (s),veh/h/ln1781 } & 0 & 1738 & 1781 & 1870 & 1595 & 1781 & 1945 & 1648 & 1781 & 1777 & 1850\end{array}$ $\begin{array}{llllllllllllll}\text { Q Serve }\left(g \_s\right), ~ s & 7.0 & 0.0 & 6.1 & 6.3 & 1.3 & 15.4 & 0.5 & 28.0 & 3.7 & 17.2 & 20.5 & 20.5\end{array}$ $\begin{array}{llllllllllllll}\text { Cycle Q Clear(g_c), s } & 7.0 & 0.0 & 6.1 & 6.3 & 1.3 & 15.4 & 0.5 & 28.0 & 3.7 & 17.2 & 20.5 & 20.5\end{array}$ $\begin{array}{lllllllllll}\text { Prop In Lane } & 1.00 & 0.42 & 1.00 & & 1.00 & 1.00 & 1.00 & 1.00 & 0.04\end{array}$

 $\begin{array}{lllllllllllll}\text { V/C Ratio(X) } & 0.89 & 0.00 & 0.37 & 0.80 & 0.08 & 0.67 & 0.03 & 0.72 & 0.13 & 0.96 & 0.48 & 0.48\end{array}$ Avail Cap(c_a), veh/h 132 $\begin{array}{lllllllllllllllll} & 1.000\end{array}$ Uniform Delay (d) s/veh $49.6 \begin{array}{llllllllllllll} & 0.0 & 39.6 & 49.2 & 37.5 & 17.3 & 38.0 & 24.6 & 17.8 & 507 & 352 & 352\end{array}$

$$
\text { Unsig. Movement Delay, } s / v e h
$$



| nGrp LOS | F | A | D | E | D | B | D | C | B | F | D | D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


|  | A | D | E | D | B | D | C | B | F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Vol, veh/h | 228 |  | 492 |  | 722 |  |  | 1033 |  |
| Approach Delay, s/veh | 68.7 |  | 31.6 |  | 28.3 |  | 51.5 |  |  |


| Approach Delay, s/veh | 68.7 | 31.6 | 28.3 | 51.5 |
| :--- | ---: | ---: | ---: | ---: |
| Approach LOS | E | C | C | D |


| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration $(G+Y+R c)$ 810.0 | 525 | 120 | 22.5 | 22.4 | 51.1 | 120 | 22.5 |  |


|  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |

$\begin{array}{llllllllll} & & & 8.0\end{array}$
$\begin{array}{llllllll}\text { Max Green Setting (Gmaxp. } & 33.4 & 9.0 & 3 . & 5.0 & 40 & 8.0 & 3.0\end{array}$
$\begin{array}{lrrrrrrr}\text { Max Q Clear Time (g_c } \mathrm{c} 1 \mathrm{mq}, 2 \mathrm{~s} & 30.0 & 8.3 & 8.1 & 2.5 & 22.5 & 9.0 & 17.4 \\ \text { Green Ext Time (p_c), s } & 0.0 & 1.3 & 0.0 & 0.6 & 0.0 & 4.5 & 0.0 \\ 1.3\end{array}$
Intersection Summary

## HCM 6th Ctrr Delay

ombos
42.4
D
${ }^{*}$ NCM NCM 6 th computational engine requires equal clearance times for the phases crossing the barrier.


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3 | 39.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement E | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations | \% | A |  | \% | F |  |  | $\dagger$ |  |  | $\dagger$ |  |  |
| Traffic Vol, veh/h | 171 | 459 | 7 | 10 | 484 | 158 | 3 | 4 | 10 | 114 | 2 | 105 |  |
| Future Vol, veh/h | 171 | 459 | 7 | 10 | 484 | 158 | 3 | 4 | 10 | 114 | 2 | 105 |  |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - |  | None | . | - | None | - |  | None |  |
| Storage Length | 65 | - | - | 75 | - | - |  | - |  | - |  |  |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - |  | 0 |  | - | 0 |  |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 171 | 459 | 7 | 10 | 484 | 158 | 3 | 4 | 10 | 114 | 2 | 105 |  |
| Major/Minor Majer | Major1 |  | Major2 |  |  | Minor 1 |  | Minor2 |  |  |  | $563$ |  |
| Conflicting Flow All | 642 | 0 | 0 | 466 | 0 | 01442 |  | 1467 | 463 | 1395 | 1391 |  | 563 |
| Stage 1 | - | - | - |  | - | - | 805 | 805 | - | 583 | 583 |  |  |
| Stage 2 | - | - | - |  | - | - | 637 | 662 | - | 812 | 808 |  |  |
| Critical Hdwy 4 | 4.12 | - | - | 4.12 | - | - | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 |  |  |
| Critical Hdwy Stg 2 | - | - |  |  | - | - | 6.12 | 5.52 |  | 6.12 | 5.52 |  |  |
| Follow-up Hdwy 2.2 | 2.218 | - | $\begin{array}{r} -2.218 \\ -\quad 1095 \end{array}$ |  | - |  | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 |  |
| Pot Cap-1 Maneuver | 943 | - |  |  | - | - | 110 | 128 | 599 | 119 | 142 | 526 |  |
| Stage 1 | - | - |  | - - | - | - | 376 | 395 |  | 498 | 499 |  |  |
| Stage 2 | - | - | - - |  | - | - | 465 | 459 |  | 373 | 394 |  |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 943 | - | - | 1095 | - | - | 74 | 104 | 599 | ~97 | 115 | 526 |  |
| Mov Cap-2 Maneuver | - | - |  | - - | - | - | 74 | 104 | - | ~97 | 115 | - |  |
| Stage 1 | - | - | - - |  |  | - | 308 | 324 |  | 408 | 495 |  |  |
| Stage 2 | - | - | - - |  | - | - | 367 | 455 | - | 297 | 323 | - |  |
| Approach | EB |  | WB |  |  | NB |  |  | SB |  |  |  |  |
| HCM Control Delay, s | 2.6 |  | 0.1 |  |  | 27.3 |  |  | 263.2 |  |  |  |  |
| HCM LOS |  |  |  |  |  | D |  |  | F |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |  |  |  |  |
| Capacity (veh/h) |  | 178 | $\begin{array}{r} 943 \\ 0.181 \end{array}$ |  |  | 1095 | - | - 159 |  |  |  |  |  |
| HCM Lane V/C Ratio |  | 0.096 |  | - |  | 0.009 |  | - | 1.39 |  |  |  |  |
| HCM Control Delay (s) |  | 27.3 | 9.7 |  | - | 8.3 |  |  | 263.2 |  |  |  |  |
| HCM Lane LOS |  | D | A |  |  | A |  | - | F |  |  |  |  |
| HCM 95th \%tile Q(veh) |  | 0.3 | 0.7 - |  |  | 0 | - | - 13.8 |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ : Volume exceeds capac | acity | \$: De | lay exc | ceds 30 |  | +: Com | putatio | Not De | efined | * All | major | volume | in platoon |


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| HCM 6th Signalized Intersection Summary <br> 5: Hearn Ave \& Dutton Meadow |  |  |  |  |  |  |  |  |  |  | 02/11/2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{ }$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\stackrel{ }{ }$ |  | \% | $\uparrow$ |  |  | $\uparrow$ | * |  |  |  |
| Traffic Volume (veh/h) | 0 | 571 | 79 | 388 | 466 | 0 | 134 | 0 | 468 | 0 | 0 | 0 |
| Future Volume (veh/h) | 0 | 571 | 79 | 388 | 466 | 0 | 134 | 0 | 468 | 0 | 0 | 0 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1870 | 1870 | 1870 | 1870 | 0 | 1870 | 1870 | 1870 |  |  |  |
| Adj Flow Rate, veh/h | 0 | 571 | 79 | 388 | 466 | 0 | 134 | 0 | 468 |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Percent Heavy Veh, \% | 0 | 2 | 2 | 2 | 2 | 0 | 2 | 2 | 2 |  |  |  |
| Cap, veh/h | 0 | 647 | 90 | 410 | 1324 | 0 | 275 | 0 | 609 |  |  |  |
| Arrive On Green | 0.00 | 0.40 | 0.40 | 0.23 | 0.71 | 0.00 | 0.15 | 0.00 | 0.15 |  |  |  |
| Sat Flow, veh/h | 0 | 1608 | 222 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Grp Volume(v), veh/h | 0 | 0 | 650 | 388 | 466 | 0 | 134 | 0 | 468 |  |  |  |
| Grp Sat Flow(s),veh/h/n | 0 | 0 | 1830 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Q Serve(g_s), s | 0.0 | 0.0 | 15.7 | 10.3 | 4.6 | 0.0 | 3.3 | 0.0 | 1.3 |  |  |  |
| Cycle Q Clear (__c), s | 0.0 | 0.0 | 15.7 | 10.3 | 4.6 | 0.0 | 3.3 | 0.0 | 1.3 |  |  |  |
| Prop In Lane | 0.00 |  | 0.12 | 1.00 |  | 0.00 | 1.00 |  | 1.00 |  |  |  |
| Lane $\operatorname{Grp} \operatorname{Cap}(\mathrm{c})$, veh/h | 0 | 0 | 736 | 410 | 1324 | 0 | 275 | 0 | 609 |  |  |  |
| V/C Ratio(X) | 0.00 | 0.00 | 0.88 | 0.95 | 0.35 | 0.00 | 0.49 | 0.00 | 0.77 |  |  |  |
| Avail Cap(c_a), veh/h | 0 | 0 | 819 | 410 | 1385 | 0 | 671 | 0 | 961 |  |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter(l) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |  |  |  |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 13.2 | 18.1 | 2.7 | 0.0 | 18.5 | 0.0 | 12.9 |  |  |  |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 10.4 | 30.8 | 0.2 | 0.0 | 1.3 | 0.0 | 2.1 |  |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \%ile BackOfQ(50\%),veh/n | 0.0 | 0.0 | 7.2 | 7.2 | 0.7 | 0.0 | 1.3 | 0.0 | 3.7 |  |  |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 0.0 | 0.0 | 23.6 | 49.0 | 2.9 | 0.0 | 19.8 | 0.0 | 14.9 |  |  |  |
| LnGrp LOS | A | A | C | D | A | A | B | A | B |  |  |  |
| Approach Vol, veh/h |  | 650 |  |  | 854 |  |  | 602 |  |  |  |  |
| Approach Delay, s/veh |  | 23.6 |  |  | 23.8 |  |  | 16.0 |  |  |  |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  |  |  |
| Timer - Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 14.6 | 22.8 |  |  |  | 37.4 |  | 10.4 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.6 | *3.6 |  |  |  | 3.6 |  | 3.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 11.0 | *21 |  |  |  | 35.4 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 12.3 | 17.7 |  |  |  | 6.6 |  | 5.3 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 1.5 |  |  |  | 3.2 |  | 2.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 21.5 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |


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| :--- | ---: |
| Stony Oaks TIS | Page 5 |


| HCM 6th Signalized I 1：Stony Point Rd \＆N | nters North | ction <br> oint P | Summ wwy |  |  |  |  |  |  |  |  | 02／11／2021 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | $\geqslant$ | $\downarrow$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | 7 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ |  | F |  |  |  | \％ | 个t |  | \％ | 个t |  |
| Traffic Volume（veh／h） | 130 | 0 | 424 | 0 | 0 | 0 | 174 | 857 | 0 | 0 | 1045 | 43 |
| Future Volume（veh／h） | 130 | 0 | 424 | 0 | 0 | 0 | 174 | 857 | 0 | 0 | 1045 | 43 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  |  |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／n | 1870 | 0 | 1870 |  |  |  | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 130 | 0 | 424 |  |  |  | 174 | 857 | 0 | 0 | 1045 | 43 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 0 | 2 |  |  |  | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 171 | 0 | 736 |  |  |  | 807 | 2966 | 0 | 61 | 1506 | 62 |
| Arrive On Green | 0.10 | 0.00 | 0.10 |  |  |  | 0.74 | 1.00 | 0.00 | 0.00 | 0.43 | 0.43 |
| Sat Flow，veh／h | 1781 | 0 | 1585 |  |  |  | 1781 | 3647 | 0 | 644 | 3478 | 143 |
| Grp Volume（v），veh／h | 130 | 0 | 424 |  |  |  | 174 | 857 | 0 | 0 | 534 | 554 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1585 |  |  |  | 1781 | 1777 | 0 | 644 | 1777 | 1845 |
| Q Serve（g＿s），s | 8.4 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 28.7 | 28.7 |
| Cycle Q Clear（g＿c），s | 8.4 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 28.7 | 28.7 |
| Prop In Lane | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 0.00 | 1.00 |  | 0.08 |
| Lane Grp Cap（c），veh／h | 171 | 0 | 736 |  |  |  | 807 | 2966 | 0 | 61 | 769 | 799 |
| V／C Ratio（X） | 0.76 | 0.00 | 0.58 |  |  |  | 0.22 | 0.29 | 0.00 | 0.00 | 0.69 | 0.69 |
| Avail Cap（c＿a），veh／h | 433 | 0 | 970 |  |  |  | 807 | 2966 | 0 | 61 | 769 | 799 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 |  |  |  | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 |  |  |  | 0.75 | 0.75 | 0.00 | 0.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 52.0 | 0.0 | 23.1 |  |  |  | 6.0 | 0.0 | 0.0 | 0.0 | 27.1 | 27.1 |
| Incr Delay（d2），s／veh | 2.6 | 0.0 | 0.3 |  |  |  | 0.0 | 0.2 | 0.0 | 0.0 | 5.1 | 4.9 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 3.8 | 0.0 | 13.9 |  |  |  | 1.0 | 0.1 | 0.0 | 0.0 | 12.7 | 13.2 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 54.7 | 0.0 | 23.4 |  |  |  | 6.1 | 0.2 | 0.0 | 0.0 | 32.2 | 32.0 |
| LnGrp LOS | D | A | C |  |  |  | A | A | A | A | C | C |
| Approach Vol，veh／h |  | 554 |  |  |  |  |  | 1031 |  |  | 1088 |  |
| Approach Delay，s／veh |  | 30.7 |  |  |  |  |  | 1.2 |  |  | 32.1 |  |
| Approach LOS |  | C |  |  |  |  |  | A |  |  | C |  |
| Timer－Assigned Phs |  | 2 |  | 4 | 5 | 6 |  |  |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{RC}$ ）， S |  | 102.4 |  | 15.6 | 47.4 | 55.0 |  |  |  |  |  |  |
| Change Period（ $Y+R \mathrm{C}$ ），$s$ |  | 3.9 |  | 4.3 | 3.9 | ＊ 3.9 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s |  | 81.1 |  | 28.7 | 27.0 | ＊51 |  |  |  |  |  |  |
| Max Q Clear Time（g＿c ${ }^{\text {c }}$ ），s |  | 2.0 |  | 10.4 | 2.0 | 30.7 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s |  | 6.9 |  | 0.9 | 0.2 | 6.8 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 19.9 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier．

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | A |  | ${ }^{*}$ | $\uparrow$ | 「 | \％ | $\uparrow$ | 7 | \％ | 个 ${ }_{\text {a }}$ |  |
| Traffic Volume（veh／h） | 42 | 32 | 23 | 146 | 40 | 322 | 40 | 713 | 136 | 296 | 845 | 29 |
| Future Volume（veh／h） | 42 | 32 | 23 | 146 | 40 | 322 | 40 | 713 | 136 | 296 | 845 | 29 |
| Initial $Q(Q b)$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／n | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1945 | 1945 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 42 | 32 | 23 | 146 | 40 | 322 | 40 | 713 | 136 | 296 | 845 | 29 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 54 | 51 | 36 | 136 | 178 | 720 | 55 | 715 | 606 | 640 | 2491 | 85 |
| Arrive On Green | 0.03 | 0.05 | 0.05 | 0.08 | 0.10 | 0.10 | 0.03 | 0.37 | 0.37 | 0.72 | 1.00 | 1.00 |
| Sat Flow，veh／h | 1781 | 1012 | 727 | 1781 | 1870 | 1585 | 1781 | 1945 | 1648 | 1781 | 3505 | 120 |
| Grp Volume（v），veh／h | 42 | 0 | 55 | 146 | 40 | 322 | 40 | 713 | 136 | 296 | 428 | 446 |
| Grp Sat Flow（s），veh／h／n | 1781 | 0 | 1739 | 1781 | 1870 | 1585 | 1781 | 1945 | 1648 | 1781 | 1777 | 1849 |
| Q Serve（g＿s），s | 2.8 | 0.0 | 3.7 | 9.0 | 2.3 | 1.9 | 2.6 | 43.2 | 6.7 | 8.3 | 0.0 | 0.0 |
| Cycle Q Clear（g＿c），s | 2.8 | 0.0 | 3.7 | 9.0 | 2.3 | 1.9 | 2.6 | 43.2 | 6.7 | 8.3 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.42 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.07 |
| Lane Grp Cap（c），veh／h | 54 | 0 | 87 | 136 | 178 | 720 | 55 | 715 | 606 | 640 | 1263 | 1314 |
| V／C Ratio（X） | 0.78 | 0.00 | 0.63 | 1.07 | 0.22 | 0.45 | 0.73 | 1.00 | 0.22 | 0.46 | 0.34 | 0.34 |
| Avail Cap（c＿a），veh／h | 106 | 0 | 457 | 136 | 523 | 1013 | 106 | 715 | 606 | 640 | 1263 | 1314 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.78 | 0.78 | 0.78 |
| Uniform Delay（d），s／veh | 56.8 | 0.0 | 55.0 | 54.5 | 49.4 | 12.6 | 56.7 | 37.2 | 25.7 | 11.8 | 0.0 | 0.0 |
| Incr Delay（d2），s／veh | 21.1 | 0.0 | 7.4 | 98.6 | 0.6 | 0.4 | 6.6 | 32.8 | 0.9 | 0.2 | 0.6 | 0.5 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh | ／111． 6 | 0.0 | 1.8 | 7.7 | 1.1 | 4.3 | 1.3 | 26.1 | 2.8 | 2.5 | 0.2 | 0.2 |
| Unsig．Movement Delay | ，s／veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 77.9 | 0.0 | 62.4 | 153.1 | 50.0 | 13.0 | 63.3 | 70.1 | 26.6 | 11.9 | 0.6 | 0.5 |
| LnGrp LOS | E | A | E | F | D | B | E | E | C | B | A | A |
| Approach Vol，veh／h |  | 97 |  |  | 508 |  |  | 889 |  |  | 1170 |  |
| Approach Delay，s／veh |  | 69.1 |  |  | 56.2 |  |  | 63.1 |  |  | 3.4 |  |
| Approach LOS |  | E |  |  | E |  |  | E |  |  | A |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{RC}$ ）， | ， 77 | 48.1 | 13.0 | 9.8 | 6.7 | 88.6 | 7.6 | 15.2 |  |  |  |  |
| Change Period（ $Y+R \mathrm{C}$ ）， | s 4.7 | ＊4．7 | 4.0 | 3.9 | 3.0 | 4.7 | 4.0 | ＊ 4 |  |  |  |  |
| Max Green Setting（Gma | axte 3 | ＊ 43 | 9.0 | 31.0 | 7.0 | 55.4 | 7.0 | ＊ 33 |  |  |  |  |
| Max Q Clear Time（g＿c + | ＋110，38 | 45.2 | 11.0 | 5.7 | 4.6 | 2.0 | 4.8 | 4.3 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.3 | 0.0 | 0.0 | 0.2 | 0.0 | 6.1 | 0.0 | 1.4 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 35.8 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

[^5]

| PM Baseline Plus Project | Synchro 11 Report |
| :--- | ---: |
| Stony Oaks TIS | Page 3 |



| HCM 6th Signalized Intersection Summary <br> 5: Hearn Ave \& Dutton Meadow |  |  |  |  |  |  |  |  |  |  | 02/11/2021 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{ }$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\hat{}$ |  | \% | $\uparrow$ |  |  | $\uparrow$ | * |  |  |  |
| Traffic Volume (veh/h) | 0 | 454 | 89 | 289 | 651 | 0 | 128 | 0 | 314 | 0 | 0 | 0 |
| Future Volume (veh/h) | 0 | 454 | 89 | 289 | 651 | 0 | 128 | 0 | 314 | 0 | 0 | 0 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  |  |  |
| Adj Sat Flow, veh/h/ln | 0 | 1870 | 1870 | 1870 | 1870 | 0 | 1870 | 1870 | 1870 |  |  |  |
| Adj Flow Rate, veh/h | 0 | 454 | 89 | 289 | 651 | 0 | 128 | 0 | 314 |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Percent Heavy Veh, \% | 0 | 2 | 2 | 2 | 2 | 0 | 2 | 2 | 2 |  |  |  |
| Cap, veh/h | 0 | 576 | 113 | 357 | 1249 | 0 | 304 | 0 | 588 |  |  |  |
| Arrive On Green | 0.00 | 0.38 | 0.38 | 0.20 | 0.67 | 0.00 | 0.17 | 0.00 | 0.17 |  |  |  |
| Sat Flow, veh/h | 0 | 1519 | 298 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Grp Volume(v), veh/h | 0 | 0 | 543 | 289 | 651 | 0 | 128 | 0 | 314 |  |  |  |
| Grp Sat Flow(s),veh/h/n | 0 | 0 | 1817 | 1781 | 1870 | 0 | 1781 | 0 | 1585 |  |  |  |
| Q Serve(g_s), s | 0.0 | 0.0 | 10.8 | 6.3 | 7.2 | 0.0 | 2.6 | 0.0 | 0.0 |  |  |  |
| Cycle Q Clear (__c), s | 0.0 | 0.0 | 10.8 | 6.3 | 7.2 | 0.0 | 2.6 | 0.0 | 0.0 |  |  |  |
| Prop In Lane | 0.00 |  | 0.16 | 1.00 |  | 0.00 | 1.00 |  | 1.00 |  |  |  |
| Lane $\operatorname{Grp} \operatorname{Cap}(\mathrm{c})$, veh/h | 0 | 0 | 689 | 357 | 1249 | 0 | 304 | 0 | 588 |  |  |  |
| V/C Ratio(X) | 0.00 | 0.00 | 0.79 | 0.81 | 0.52 | 0.00 | 0.42 | 0.00 | 0.53 |  |  |  |
| Avail Cap(c_a), veh/h | 0 | 0 | 1043 | 524 | 1762 | 0 | 786 | 0 | 1017 |  |  |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  |
| Upstream Filter(l) | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 |  |  |  |
| Uniform Delay (d), s/veh | 0.0 | 0.0 | 11.2 | 15.6 | 3.5 | 0.0 | 15.1 | 0.0 | 10.1 |  |  |  |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 2.4 | 3.6 | 0.3 | 0.0 | 0.9 | 0.0 | 0.8 |  |  |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| \%ile BackOfQ(50\%),veh/n | 0.0 | 0.0 | 3.7 | 2.5 | 1.0 | 0.0 | 0.9 | 0.0 | 1.7 |  |  |  |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 0.0 | 0.0 | 13.6 | 19.2 | 3.8 | 0.0 | 16.0 | 0.0 | 10.8 |  |  |  |
| LnGrp LOS | A | A | B | B | A | A | B | A | B |  |  |  |
| Approach Vol, veh/h |  | 543 |  |  | 940 |  |  | 442 |  |  |  |  |
| Approach Delay, s/veh |  | 13.6 |  |  | 8.5 |  |  | 12.3 |  |  |  |  |
| Approach LOS |  | B |  |  | A |  |  | B |  |  |  |  |
| Timer - Assigned Phs | 1 | 2 |  |  |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 11.8 | 19.1 |  |  |  | 30.8 |  | 10.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 3.6 | *3.6 |  |  |  | 3.6 |  | 3.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 12.0 | *23 |  |  |  | 38.4 |  | 18.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 8.3 | 12.8 |  |  |  | 9.2 |  | 4.6 |  |  |  |  |
| Green Ext Time (p_c), s | 0.2 | 2.7 |  |  |  | 5.0 |  | 1.5 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr Delay |  |  | 10.8 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |


| PM Baseline Plus Project | Synchro 11 Report |
| :--- | ---: |
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## Appendix C

## SCTA Model VMT per Capita Map



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## SCTA Regional Model (Fall 2020) VMT per Capita by Traffic Analysis Zone




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## Appendix D

## Emergency Vehicle Access Exhibits



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| Sonoma County Fire Truckeet |  |
| :--- | :--- |
| Width | $: 8.00$ |
| Track | $\vdots .911$ |
| Lockt Lock Time | $\vdots .0$ |
| Steering Angle | $\vdots 38.8$ |



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## Appendix E

Signal Warrant Spreadsheets


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## Warrant 3: Peak-Hour Volumes and Delay

Hearn Avenue \& Burbank Avenue Santa Rosa

Project Name: Stony Oaks TIS

Intersection: 4

| Major Street | Minor Street |
| :---: | :---: |
| Hearn Avenue | Burbank Avenue |
| E-W | N-S |
| 1 | 1 |
| 30 | 25 |

No
Wednesday, September 11, 2019
AM Baseline

| Warrant 3 Met?: Met when either Condition $A$ or $B$ is met | Yes |
| :---: | :---: |
| Condition A: Met when conditions A1, A2, and A3 are met | Met |
| Condition A1 | Met |
| The total delay experienced by traffic on one minor street approach (one direction only) controlled by a STOP sign equals or exceeds four vehicle-hours for a one lane approach, or five vehicle-hours for a two-lane approach |  |
| Minor Approach Delay: 29.81 vehicle-hours |  |
| Condition A2 | Met |

再 100 vph for one moving lane of traffic of 150 vph for two moving lanes

$$
\text { Minor Approach Volume: } 261 \text { vph }
$$

## Condition A3

The total entering volume serviced during the hour equals or exceeds 800 vph for intersections with four or more appraches or 650 vph for intersections with three approaches

Total Entering Volume: 1603 vph
Condition B
The plotted point falls above the curve


## Warrant 3: Peak-Hour Volumes and Delay

Hearn Avenue \& Burbank Avenue Santa Rosa

Project Name: Stony Oaks TIS

Intersection: 4

| Major Street | Minor Street |
| :---: | :---: |
| Hearn Avenue | Burbank Avenue |
| E-W | N-S |
| 1 | 1 |
| 30 | 25 |

No
Wednesday, September 11, 2019
PM Baseline

| Warrant 3 Met?: Met when either Condition A or B is met |  | Yes |
| :---: | :---: | :---: |
| Condition A: Met when conditions A1, A2, and | met | Met |
| Condition A1 |  | Met |
| The total delay experienced by traffic on one minor street approach (one direction only) controlled by a STOP sign equals or exceeds four vehicle-hours for a one lane approach, or five vehicle-hours for a two-lane approach |  |  |
| Minor Approach Delay | 13.51 vehicle-hours |  |
| Condition A2 |  | Met |

隹 100 vph for one moving lane of traffic of 150 vph for two moving lanes

$$
\text { Minor Approach Volume: } 239 \text { vph }
$$

## Condition A3

The total entering volume serviced during the hour equals or exceeds 800 vph for intersections with four or more appraches or 650 vph for intersections with three approaches

Total Entering Volume: 1563 vph
Condition B
The plotted point falls above the curve


## Warrant 3: Peak-Hour Volumes and Delay

Hearn Avenue \& Burbank Avenue Santa Rosa
Street Name
Direction
Number of Lanes
Approach Speed

Population less than 10,000?
Date of Count:
Scenario:

Project Name: Stony Oaks TIS

Intersection: 4

| Major Street | Minor Street |
| :---: | :---: |
| Hearn Avenue | Burbank Avenue |
| E-W | N-S |
| 1 | 1 |
| 30 | 25 |

No
Wednesday, September 11, 2019
AM Baseline Plus Project

| Warrant 3 Met?: Met when either Condition A or B is met |  |
| :--- | :--- |
| Condition A: Met when conditions A1, A2, and A3 are met | Yes |
| Condition A1 |  |
| The total delay experienced by traffic on one minor street approach (one direction only) |  |
| controlled by a STOP sign equals or exceeds four vehicle-hours for a one lane approach, |  |
| or five vehicle-hours for a two-lane approach |  |
| $\quad$ Minor Approach Delay: |  |
| Condition A2 <br> The volume on the same minor street approach (one direction only) equals or exceeds |  |

velume on the same minor street approach (one direction only) equals or exceeds 100 vph for one moving lane of traffic of 150 vph for two moving lanes

$$
\text { Minor Approach Volume: } 261 \text { vph }
$$

## Condition A3

The total entering volume serviced during the hour equals or exceeds 800 vph for intersections with four or more appraches or 650 vph for intersections with three approaches

Total Entering Volume: 1623 vph

## Condition B

The plotted point falls above the curve


## Warrant 3: Peak-Hour Volumes and Delay

Hearn Avenue \& Burbank Avenue Santa Rosa
Street Name
Direction
Number of Lanes
Approach Speed

Population less than 10,000?
Date of Count:
Scenario:

Project Name: Stony Oaks TIS

Intersection: 4

| Major Street | Minor Street |
| :---: | :---: |
| Hearn Avenue | Burbank Avenue |
| E-W | N-S |
| 1 | 1 |
| 30 | 25 |

No
Wednesday, September 11, 2019
PM Baseline Plus Project

| Warrant 3 Met?: Met when either Condition A or B is met |  |
| :--- | :--- |
| Condition A: Met when conditions A1, A2, and A3 are met | Yes |
| Condition A1 |  |
| The total delay experienced by traffic on one minor street approach (one direction only) |  |
| controlled by a STOP sign equals or exceeds four vehicle-hours for a one lane approach, |  |
| or five vehicle-hours for a two-lane approach |  |
| $\quad$ Minor Approach Delay: 14.89 vehicle-hours |  |
| Condition A2 |  |
| The volume on the same minor street approach (one direction only) equals or exceeds |  | 100 vph for one moving lane of traffic of 150 vph for two moving lanes

$$
\text { Minor Approach Volume: } 239 \text { vph }
$$

## Condition A3

The total entering volume serviced during the hour equals or exceeds 800 vph for intersections with four or more appraches or 650 vph for intersections with three approaches

Total Entering Volume: 1588 vph
Condition B
The plotted point falls above the curve


## Appendix F

## Proportionate Share Calculations



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## Equitable Share Calculations <br> Hearn Avenue/Burbank Avenue

## AM Peak Hour Southbound Approach Delay (seconds)

| Existing | 62.4 |
| :--- | ---: |
| Baseline (no project) | 244.5 |
| Baseline + Project | 263.2 |
| Project Delay (D) | 18.7 |

## Description of Project Improvement:

Install traffic signal

## Calculation of Project Share

```
P=D / (DB - DE)
```

where:
P = Equitable Share
D = Project added delay during the affected peak hour DB = Baseline plus Project Delay
DE = Existing Delay

| D | 18.7 |  |
| :--- | ---: | ---: |
| DB | 263.2 |  |
| DE | 62.4 |  |
| P | $\mathbf{9 . 3 \%}$ |  |
|  |  |  |
| Total Estimated Cost of Improvements | $\$ 320,000$ |  |
| Equitable Share Contribution | $\$ \mathbf{2 9 , 7 6 0}$ |  |



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[^0]:    Reference: Highway Capacity Manual, Transportation Research Board, $6{ }^{\text {th }}$ Edition, 2018

[^1]:    AM Existing
    Synchro 11 Report
    Stony Oaks TIS

[^2]:    PM Existing
    Synchro 11 Report
    Stony Oaks TIS

[^3]:    AM Baseline
    Synchro 11 Repor
    Page 4

[^4]:    ＊HCM 6th computational engine requires equal clearance times for the phases crossing the barrier

[^5]:    ＊HCM 6 th computational engine requires equal clearance times for the phases crossing the barrier

